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# Pulp Mill Effluent Treatment Using Plasma Obtained by High Voltage Electrolysis

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Effluents from pulp mills have a high organic load and can still contain high organic biorecalcitrant material that is harmful to the aquatic environment, even after undergoing biological treatment in effluent treatment plants. This study presents a novel treatment method tested on effluents (prior to and after biotreatment) from a Brazilian kraft pulp mill, based on hydroxyl radical production and hydrogen peroxide obtained by plasma generated by high-voltage electrolysis. These species present significant oxidation potential that could enable the complete breakdown of the organic matter. From the application of plasma to treat pulp mill effluent for a 7-hour period, it was obtained a chemical oxygen demand (COD) removal between 88.2 and 99.7%, total organic carbon (TOC) removal of 90.3 to 95.6%, and a color removal of 95.0 to 98.0%. The final pH of the treated effluent was 11.6 to 11.9. The results obtained in this study showed that the high-tension plasma treatment, applied on effluent from kraft pulp mills before and after biological treatment, can be an attractive alternative.

Keywords: effluent, pulp industry, electric plasma, high voltage

# Introduction

The pollution of water bodies by industrial effluent discharges is a problem in various regions around the world. Industrial effluent from bleached kraft pulp mills is a potential polluter. It is produced in large quantities during industrial process and can still present significant pollution risks even after primary and secondary biological treatment. In the 1990's, average water use in North American pulp mills was 60 m<sup>3</sup> *per* ton of dry pulp (adt) produced.<sup>1</sup> Modern mills reduced the specific water consumption to approximately 25 m<sup>3</sup> adt<sup>-1,2</sup> Given this, a mill that produces 5000 adt day<sup>-1</sup> would consume a water volume of 125,000 m<sup>3</sup> day<sup>-1</sup>, equivalent to the water consumption of a city with one million people.

Effluents are rich in organic matter coming from wood (chemical oxygen demand (COD) > 1200 mg L<sup>-1</sup> and 5-day biochemical oxygen demand (BOD5) > 350 mg L<sup>-1</sup>) and the effluent treatment plant is normally composed of primary treatment (sedimentation) for suspended solids removal followed by an aerobic biological treatment system, an

activated sludge process being the most commomly used. However, this treatment sequence is not sufficient to remove recalcitrant organics or color.<sup>3</sup>

Therefore, there is a need to look for new treatment options that can be combined with the already existing ones or even replace these, to obtain a final effluent less harmful to the environment. An innovative treatment for this effluent could be the use of plasma obtained through high tension and low current electrolysis.

Plasma is produced via potential difference between two electrodes immersed in an aqueous solution, with plasma formation at the anode, where chemical reactions occur under non-faradaic effects, producing, in addition to the hydroxyl radical (HO•), various other types of reactive agents such as O•, HO<sub>2</sub>•, H•, H<sub>2</sub>O<sub>2</sub>, H<sub>2</sub> and O<sub>2</sub>.<sup>4-7</sup>

The formation of some of these reactive agents is shown in equations 1 to 5:

$\mathrm{H_2O} \rightarrow \mathrm{OH} \bullet + \mathrm{H} \bullet$	(1)
$\mathrm{H}^{\bullet} + \mathrm{H}^{\bullet} \to \mathrm{H}_2$	(2)
$\bullet OH + \bullet OH \rightarrow H_2O_2$	(3)
$\bullet OH + H_2O_2 \rightarrow HO_2 \bullet + H_2O$	(4)
•OH + HO <sub>2</sub> • $\rightarrow$ H <sub>2</sub> O + O <sub>2</sub>	(5)

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The use of plasma to breakdown diverse organic compounds has been reported in the literature, amongst these, alquilbenzenosulfonate, which obtained a 90% mineralization of these compounds.<sup>8</sup> Regarding monochlorophenol compounds, the results showed a 100% breakdown within four hours applying plasma.<sup>9</sup>

For the breakdown of dyes, in addition to the use of plasma, studies also investigated the addition of  $Fe^{2+}$  to the solution, as a catalyzing agent for breakdown, which showed more efficient and faster results.<sup>10,11</sup> Wang *et al.*<sup>12</sup> reports the use of plasma in the treatment of various wastewater, for example, degradation of dyes used in the textile dyeing industry.

The main purpose of the present study was to evaluate the use of plasma obtained by high voltage electrolysis to treat kraft pulp mill effluents.

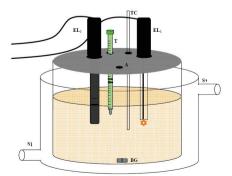
# Experimental

#### Effluent sampling and preservation

The effluents were collected in a Brazilian bleached kraft pulp mill with an ECF (elemental chlorine free) bleaching sequence. The samples were collected before and after the effluent treatment plant, which consisted of an initial clarifier followed by an activated sludge biological process. The effluents were kept under refrigeration (4 °C).

#### Experimental design

The system shown in Figure 1 was used, composed of two electrodes to obtain the plasma, a graphite electrode (cathode) and a platinum microelectrode (anode), with a 0.5 mm diameter and exposure of 2.0 mm of platinum in contact with the effluent. A thermostatized bath (Frigomix, B Braun Biotech International), a temperature control (Thermomix BM-S, B. Braun Biotech International) for



**Figure 1.** Cell scheme:  $EL_1$ , platinum electrode;  $EL_2$ , graphite electrode; A, orifice; TC, capillary tube for sampling; T, thermometer;  $S_1$  and  $S_2$ , in and out flow of water, respectively; BG, magnetic bar.

circulation of the refrigeration water and a magnetic stirrer for the homogenization of the reaction medium were used.

The system was used to treat 300 mL of effluent from a pulp mill, before (EBBT) and after (EABT) biological treatment. A difference in potential of 585 V and a maximum current of 200 mA was applied using a high-tension source (DC Power Supply, Supplier). Under constant magnetic stirring, the plasma treatment was maintained during 30 min to 7 h. This range was chosen because after 7 h a high COD is generally observed and, therefore, the experiments are stopped. All assays were performed in duplicate.

The physical-chemical characterization of the effluents was performed according to the Standard Methods for the Examination of Water and Wastewater (1998).<sup>13</sup> The parameters indicated were: COD, total organic carbon (TOC, LAR Process Analysers AG, model Quick TOC), color, chloride (Cl<sup>-</sup>) content and pH.

## **Results and Discussion**

#### Effluent characterization

The physical-chemical characteristics of the EBBT and EABT mill effluents are presented in Table 1.

 Table 1. Physical-chemical characteristics of the EBBT and EABT mill effluents

EBBT	EABT	
$1340 \pm 18$	187 ± 16	
$207 \pm 19$	$288 \pm 10$	
$5.18 \pm 0.11$	$7.95 \pm 0.45$	
$544 \pm 3.5$	83 ± 1.1	
$275 \pm 10$	ND	
	$1340 \pm 18$ $207 \pm 19$ $5.18 \pm 0.11$ $544 \pm 3.5$	

EBBT: effluent before biological treatment; EABT: effluent after biological treatment; COD: chemical oxygen demand; HU: Hazen units; TOC: total organic carbon; ND: not determined.

The COD values for the raw and biotreated effluent are typical for this type of industry. Kamali and Khodaparast<sup>3</sup> report a COD range of 1000 to 6000 mg L<sup>-1</sup> for pulp milleffluent. Color is not affected by primary or secondary biotreatment and, therefore, each pulp mill presents different color values depending especially on their manufacturing process.

#### Plasma characterization

For the plasma system used, the following behavior of the current *versus* voltage (Figure 2) was observed.

Other authors such as Gao *et al.*<sup>11</sup> and Gupta<sup>14</sup> also reported the same behavior for the current *versus* potential

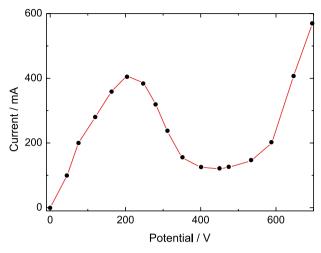


Figure 2. Current curve versus potential difference.

difference. For these authors there is an agreement in terms of the explanation for such behavior.

All authors considered the curve divided into three parts, with the current increasing in the first part, almost proportional to the increase of the applied tension. This suggests that the electrolysis obeys the law of Ohm, with the decomposition of the water and the current being stable during this phase. In the second phase (200-480 V), sparks were observed at irregular intervals and the current became unstable. This can be explained by the large quantity of heat produced near the tip of the anode, making the water around the electrode vaporize. Therefore, the current dropped off abruptly, keeping in mind the electrical resistance of the water vapor. When the tension applied went above 480 V, the current increased once again. This is due to the complete collapse of the water vapor, and the normal electrolysis spontaneously changes to the electrolysis of the luminescent discharge and the plasma formed becomes stable.

Study of the COD reduction according to time of plasma application in the effluents

The temperature of the thermostatized bath was set at 10 °C. This low value was necessary to dissipate the high heat produced by the plasma, which, according to Gupta,<sup>7</sup> is a common phenomenum considering the low volume used in a lab-scale experiment (300 mL). Effluent before (EBBT) and after (EABT) biological treatment and without any correction of pH was used. Given that the effluent used has a large electrolytic charge sufficient for the formation of the plasma, it was not necessary to add electrolytic support. The response used for the analysis was the COD value. The results are presented in Figure 3.

Based on the graphs presented in Figure 3, an exponential behavior in the breakdown of the effluent organic matter from the pulp mill was observed, finding that within 420 min this value was almost null for the EBBT.

These results show that within a retention time less than the used in the biological treatment for the activated sludge, a more satisfactory result was obtained, considering that in the effluent treated with plasma there was a drastic reduction of organic matter over the time considered.

Study of the TOC reduction with the time of plasma application in the effluent

These analyses were performed to determine the organic carbon content present in the EBBT and EABT effluents, since, contrary to the COD, the analysis of the TOC is independent of the state of oxidation of the organic matter. Additionally, it does not undergo interference from the other atoms connecting with the organic structure such as nitrogen, hydrogen, and inorganic species such as  $Fe^{2+}$ ,  $Mn^{2+}$ ,  $S^{2-}$  and  $Cl^{-}$ .

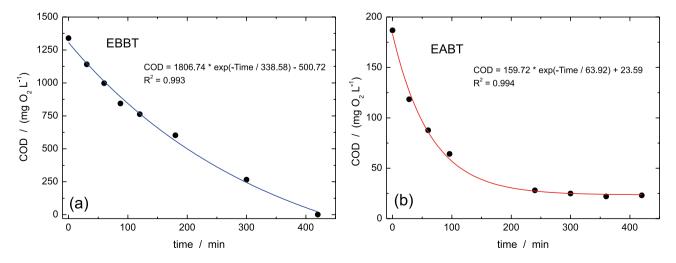


Figure 3. COD values for the effluents from pulp mill (a) EBBT and (b) EABT after the application of plasma, as a function of time.

The results obtained for the TOC analysis (Figure 4) confirm and show more clearly the exponential behavior of the breakdown of organic matter via plasma treatment, observing that the percentage of TOC removal is between 90 and 96%.

Variation of pH during the application time of the plasma in effluent

The pH value is a parameter determined by Brazilian legislation,<sup>15</sup> and should be between 6.0 and 9.0 to be able to be discharged into the environment. A study of its variability as a function of the application time of the plasma treatment was conducted. The results are presented in Figure 5.

According to the study of the pH, after treatment, the effluent to be discharged required correction to achieve pH values between 6.0 and 9.0. It is notable that for up to 3 h of treatment, this correction is facilitated, since the pH value of the effluent is around 10.

A possible explanation for the increase in pH can be deduced from the treatment of the effluent, which did not undergo addition of electrolytes. In the electrolysis of water, in the presence of an electrolyte such as sodium sulfate, for example, there is production of  $O_2$  in the anode and  $H_2$  at the cathode, with the consequent acidification and alkalinization around the electrodes, respectively. Possibly, in the electrolysis under plasma, the phenomena that occur in the platinum microelectrode do not lead to oxidation of the water, but only to oxidation of the organic matter present, in this case, in the effluent. Therefore, there is only alkalization of the medium due to the reduction of water in the cathode.

In the literature,<sup>4,12</sup> oxidation with plasma presents a decrease in the pH value. However, in these studies, organic compound solutions prepared in the laboratory were used, in other words, a much less complex matrix than an industrial cellulose effluent.

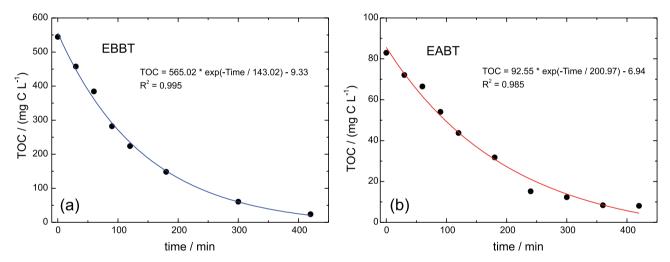


Figure 4. TOC values for the (a) EBBT and (b) EABT after the application of plasma as a function of time.

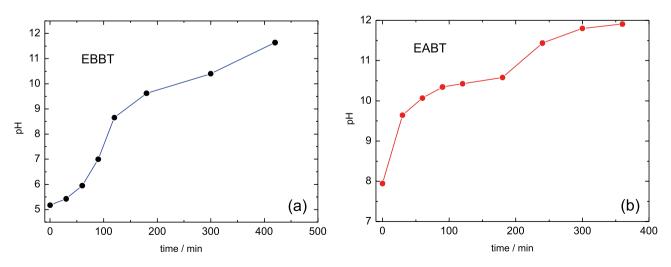


Figure 5. Variation of the pH for (a) EBBT and (b) EABT after application of plasma as a function of time.

200

150

 $R^2 = 0.981$ 

120

60

180

240

time / min

300

Study of the color removal from the application of plasma in effluent

Despite color being a parameter without a value defined by Brazilian legislation, which only states that the effluent should not alter the natural color of the receiving water body,<sup>15</sup> it is an extremely important parameter. In the majority of cases, the persistent color is due to recalcitrant organic compounds that are difficult to breakdown in the receiving water bodies. Figure 6 shows the color values for the different plasma times.

After seven hours of treatment with plasma, nearly 100% of the color of the EBBT and EABT effluents was eliminated. This result was already expected after the analysis of TOC for these effluents, since over the 7-h period, a value of 23.8 mg C L<sup>-1</sup> was obtained for the EBBT and 8.10 mg C L<sup>-1</sup> for the EABT, which are considered very low values. Given that the most significant agent responsible for the color in these types of effluent is organic

Color (mg Pt L<sup>-1</sup>) = 211.37 \* exp(-Time / 162.88) - 3.58

matter, there is an almost total removal of color resultant from its mineralization.

Spectrophotometric analysis of effluent during the plasma application time in effluent

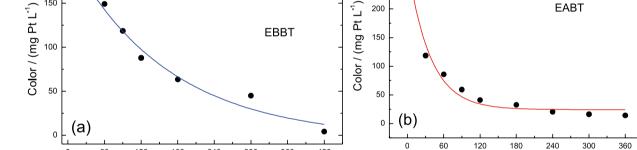
A scan wavelength between 200 to 350 nm was realized, with close ultraviolet regions, to identify the region with greatest absorbance. In Figure 7, a reduction of absorbance over the whole region studied, during the time of plasma application can clearly be observed, both in the spectra of the effluent before (EBBT) and after (EABT) biological treatment.

In Figure 7, it can be observed that the wavelength of greatest absorption, for the EBBT effluent is around 250 nm, which should be used for analysis. However, to monitor the aromatic compounds derived from lignin, absorbance readings were performed at 280 nm<sup>16</sup> to analyze the behavior of the absorbance for different plasma treatment times, as shown in Figure 8.

Color (mg Pt L<sup>1</sup>) = 258 10 \* exp(-Time / 36 84) + 24 25

time / min

EABT



420

300

250

200

 $R^2 = 0.978$ 

Figure 6. Color values for (a) EBBT and (b) EABT cellulose effluents after the application of plasma as a function of time.

360

EBBT

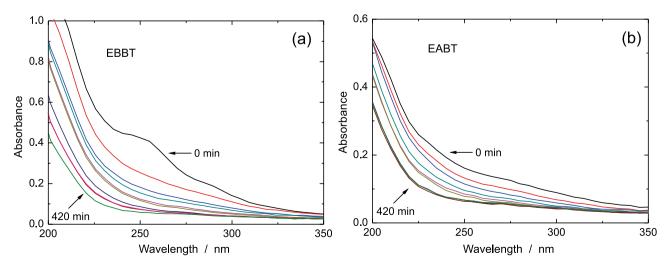


Figure 7. Absorption spectra in the UV-Vis region for the (a) EBBT and (b) EABT cellulose effluents with application of plasma as a function of time.

420

Exponential behavior tending toward zero, with an increase in the application time of the plasma was observed. This shows that aromatic compounds, one of the agents responsible for the toxicity of the effluent, are being totally oxidized as shown previously in Figure 4.

Characteristics of EBBT and EABT effluents after the application of plasma

In addition to the previously mentioned analyses, measurements of chloride concentration in the effluents before and after treatment with plasma were also performed. The results can be found on Table 2.

From the results obtained, the high pH value for both EBBT and EABT effluents after treatment with plasma was not in agreement with values cited in the literature.<sup>12</sup> However, if these effluents were reused during the first bleaching stage, after treatment, the problem of high pH value would be solved. Therefore, it would be possible to have a closed water cycle system in the kraft pulp mill, which implies in an enormous environmental gain, since the treated effluent of the mill could be used in the bleaching

sector. As expected, treatment with plasma did not change the chloride concentration.

Taking into consideration that the treated effluent volume was only 300 mL, even if the electric current was relatively low, the application time of the plasma in the effluent was 7 h, which demands high energy consumption. It is suggested that the plasma treatment be performed in a shorter time span during which the total organic carbon (TOC) would diminish to a manageable level and the rest would be consumed during the biological treatment. Therefore, the energy consumption would be much lower.

#### Conclusions

The results obtained in this study showed that the hightension plasma treatment, applied on effluent from kraft pulp mills before and after biological treatment can be an attractive alternative. More than 99% removal of COD was achieved after seven hours of treatment for EBBT and 88% for EABT effluents, which is higher than the conventional biotreatment used in pulp mills which is lower than 80%. The activated sludge processes normally used in pulp mills

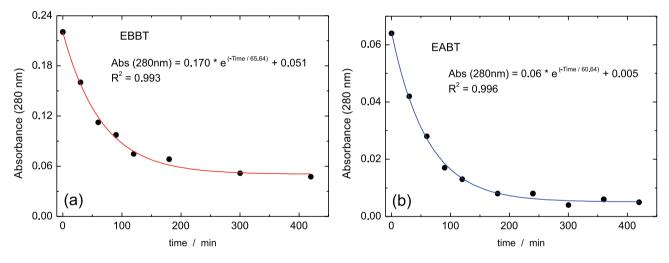


Figure 8. Absorbance at 280 nm for pulp mill effluent. (a) EBBT; (b) EABT.

Table 2. Results of the physical-chemical characterization of the effluent before (EBBT) and after (EABT) biological treatment and after seven hours of treatment with plasma

Parameter	EBBT	EBBT <sup>a</sup>	EABT	EABT <sup>a</sup>
COD / (mg L <sup>-1</sup> )	$1340 \pm 18$	$3.76 \pm 6.10$	187 ± 16	$22 \pm 1.30$
Color / HU (mg PT L-1)	$207 \pm 19$	$4 \pm 0.2$	$288 \pm 10$	$14.3 \pm 2.9$
pH	$5.18 \pm 0.11$	$11.64 \pm 0.06$	$7.95 \pm 0.45$	$11.91 \pm 0.32$
TOC / (mg C L <sup>-1</sup> )	$544 \pm 3.5$	$23.8 \pm 1.5$	83 ± 1.1	$8 \pm 2.1$
Chloride / (mg Cl- L-1)	$275 \pm 10$	$271.3 \pm 5.7$	ND	ND

<sup>a</sup>After seven hours of treatment with plasma. EBBT: effluent before biological treatment; EABT: effluent after biological treatment; COD: chemical oxygen demand; HU: Hazen units; TOC: total organic carbon; ND: not determined.

have a hydraulic retention time of between 10 to 24 h. This treatment could be an interesting alternative to reduce environmental impacts, considering that it does not require additives, reagents or catalyzers. The process does not produce sludge since all the organic matter is oxidized into  $CO_2$ . However, there is still a need to improve the energy efficiency of the process that is still considered high for the purpose of water and wastewater treatment.

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