

Reprocessability of PHB in extrusion: ATR-FTIR, tensile tests and thermal studies

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Abstract

Mechanical recycling of biodegradable plastics has to be encouraged, since the consumption of energy and raw materials can be reduced towards a sustainable development in plastics materials. In this study, the evolution of thermal and mechanical properties, as well as structural changes of poly(hydroxybutyrate) (PHB) up to three extrusion cycles were investigated. Results indicated a significant reduction in mechanical properties already at the second extrusion cycle, with a reduction above 50% in the third cycle. An increase in the crystallinity index was observed due to chemicrystallization process during degradation by chain scission. On the other hand, significant changes in the chemical structure or in thermal stability of PHB cannot be detected by Fourier transform infrared spectroscopy (FTIR) and thermogravimetric analyses (TGA), respectively.

Keywords: *biopolymer; degradation, PHB, recycling, reprocessing.*

1. Introduction

The rate of municipal solid waste (MSW) generation is rising more than the rate of urbanization around the world^[1]. By 2025, the volume of MSW generated worldwide is expected to double, reaching an amount of 2.2 billion tonnes per year^[1]. In general, plastics are of main concern because they represent between 3 and 14.3 wt% of the total MSW, most are from non-renewable sources and have relatively low recycling rates^[1-3].

A key practice to minimizing the environmental problems associated with solid waste is the practice of the 3R (Reduce, Reuse and Recycle) concept, which contributes to reduce energy and natural resources consumption, extend life cycle of products and landfills, and store carbon for a longer period, all important initiatives within the concept of sustainable development. Another alternative that has gained importance is the replacement of petroleum-based plastics by biopolymers from renewable resources, which are generally compostable and able to close the carbon cycle. According to the European Union Regulation, composting is a considered and accepted way of recovering biodegradable packaging wastes^[3]. However, recycling of biopolymers can be an alternative to composting and to reduce carbon dioxide emission, thus meeting the 3R concept. This approach not only saves energy that would be used in polymer synthesis, but also reduces costs associated with bioresources (monomers) used to produce new bioplastics and spares carbon resources. Since biopolymers are commonly used in the production

of short-life goods, recycling of these polymers becomes even more important because of the large amount of waste generated in markets, as well as insumes consumed.

Nevertheless, in the case of biodegradable plastics, there are few studies related to their recycling^[4-7]. Life cycle analysis^[8] of poly(lactic acid) (PLA), which is one of the most studied biopolymers, pointed out that despite of its low environmental impacts, this situation can worsen if recycling is not achieved. According to Shah et al.^[9], pyrolysis, solvolysis and enzymatic monomer recycling are the most promising feedstock recycling technologies for biodegradable plastics because most biopolymers have heteroatoms in their main chain, which reduce thermal stability and increase susceptibility to hydrolysis. Besides that, studies of biopolymers recyclability by multiple reprocessing are also important due to the fact that the production of biopolymer-based products may involve more than one extrusion step and mechanical recycling is the most energy efficient recycling technology.

Polyhydroxyalcanoates (PHAs) have attracted a great deal of attention due to their types, properties similar to conventional plastics, biodegradability, biocompatibility, renewability, and synthesis by biotechnological processes^[10,11]. Although their discovery occurred early, PHAs were rediscovered in the 1980s, and their use has gained increasing attraction, particularly in the last decades, as a

consequence of the reduction and limitation of the fossil fuel resources, allied with the increasing concern about the environmental issues caused by improper manipulation, use and disposal of such non-renewable materials. Among these polymers, biosynthesized polyhydroxybutyrate (PHB), the most common PHA, has a high potential to compete with commodity polymers due to its similarity in crystallinity, melting temperature, tensile strength and Young's modulus, and competitive costs^[12]. Nevertheless, high stiffness, brittleness and poor thermal stability above the melting temperature (a narrow processability window) are some of its drawbacks compared to many conventional polymers^[13-15].

Feedstock recycling of PHB has already been considered as a viable route to produce end products such as crotonic acid, linear oligomers having crotonate end groups and a cyclic trimer, as well as to produce plasticized PLA by reactive extrusion grafting of PHB degradation products onto PLA chains^[16-19]. At temperatures a little above the melting point, there is a rapid decrease in molecular weight and a subsequent production of crotonic acid as the main volatile product^[20-23]. The presence of moisture, fermentation residues, oxygen, metal and alkali catalysts also is known to favor thermal degradation^[14,24-28]. This is an important limitation for processing and consequently, to mechanical recycling. Therefore, there has been a great deal of interest in studying the thermal degradation behavior of PHB and other related poly(hydroxyalkanoate)s^[29-35]. Also studies seeking to improve the thermal stability of PHB by grafting chemicals in PHB chain^[33,36], and adding polymeric additives in PHB matrix^[37,38] have been developed.

The thermal degradation behavior of PHB has been discussed in many works^[14,20,21,30,39-42], in which a random chain scission reaction (β -elimination) involving a six-membered ring transition state (Figure 1) has been considered as the main mechanism based on typical structures of pyrolysis products, i.e., crotonic acid and oligomers with a crotonate end group, i.e., unsaturated end groups. Since the proposed mechanism is a non-radical random chain scission the conventional stabilizers and antioxidant was not efficient to prevent PHB degradation^[38].

In this work, the effect of multiple reprocessing cycles on the properties of PHB products obtained by more than one reprocessing cycle, as well as in their recyclability was evaluated. Thermal and mechanical properties were measured after each extrusion cycle, and correlated with polymer structural changes.

2. Materials and Methods

2.1 Materials

Poly(3-hydroxybutyrate) (PHB) powder, produced by bacterial fermentation, was kindly supplied by PHB Industrial S/A, Serrana-SP, Brazil, registered under the brand BIOCYLE[®] and used as received. This polymer has a melt flow index of 6.5 g/10 min (190 °C, 2.16 kg) and

number-average molecular weight (Mn) of 56,650 g.mol⁻¹, weight-average molecular weight (Mw) of 167,223 g.mol⁻¹, and polydispersity index (PDI) of 2.95, as measured by gel permeation chromatography.

2.2 Reprocessing cycles

Extrusions were carried out using an AX Plásticos (São Paulo, Brazil) single screw extruder ($\phi = 16$ mm, L/D = 26 and 90 rpm) with Maddock mixing section between the compression zone and the flow control zone up to three times. Temperature profile used was: 165, 170 and 170 °C. The neat PHB powder (virgin polymer) or pellets (extruded polymer) was dried at 60 °C under vacuum for 12 h before each processing cycle. Since it is a first approach on recyclability of PHB, no other materials/additives, such as nucleating agent or plasticizers, were used.

2.3 Compression molding

Compression molded films were prepared in a hydraulic press (capacity of 24kgf) at 170 °C for 1 min at about 10 kgf, followed by quenching in an ice-water bath.

2.4 Mechanical properties

Tensile tests were carried out according to ASTM D 882 at 25 °C and strain rate of 1%.min⁻¹ using a TA Instruments DMA, Q800. The test-specimens with dimensions around (50 × 10 × 0.075) mm were cut from films prepared by compression molding. At least 5 samples were carried out for virgin PHB and after each extrusion cycle. Results were averaged arithmetically.

2.5 Fourier transform infrared (FTIR) spectroscopy

Infrared spectra were obtained by a Nexus 470 Nicolet FTIR spectrophotometer. 32 scans, resolution of 4 cm⁻¹ and interval of 2 cm⁻¹ were used. Analyses were performed in the attenuated total reflectance mode (ATR) by direct analysis of films on SnZn crystal.

2.6 Thermogravimetric analysis (TGA)

Thermogravimetric analyses (TGA) were conducted under 50 mL.min⁻¹ of nitrogen flow, using a Shimadzu TGA 60 apparatus. The samples were heated to 600 °C at 20 °C.min⁻¹. The characteristic degradation temperatures: temperature at the maximum of the DTG curve (Tmax) and the temperature (Tx%) at which the sample loses x% of its initial weight were determined.

2.7 Differential scanning calorimetry (DSC)

Thermograms were obtained using a Shimadzu DSC 60 differential scanning calorimeter (DSC). Calibration was performed with indium and tin in the temperature range from 0 to 350 °C. The sample weight was approximately

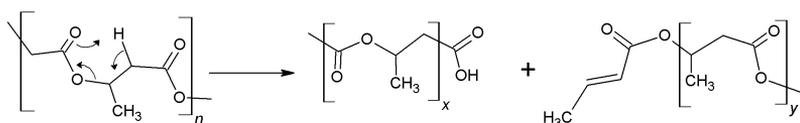


Figure 1. PHB random chain scission mechanism.

6-10 mg. All the samples were heated from 25 °C to 220 °C at 10 °C.min⁻¹ in purge flow of nitrogen at 50 mL/min. Melting enthalpies were determined using constant integration limits. The degree of crystallinity (Xc) was determined using the following equation:

$$Xc(\%) = \frac{\Delta H_m}{\Delta H_{100\%}} \times 100 \quad (1)$$

where: ΔH_m is the melting enthalpy per unit of weight of PHB samples and $\Delta H_{100\%}$ denotes enthalpy per unit weight of the 100% crystalline PHB, which is assumed to be 146 J/g^[43]. All DSC analysis was taken from the films obtained by compression molding in order to best represent the material undergoing mechanical test. This procedure has been already adopted by Srubar et al.^[44]

3. Results and Discussions

3.1 Mechanical properties

In order to assess the industrial possibility of PHB recycling, its mechanical properties must stay as stable as possible along the processing cycles. A representative tensile curve of virgin PHB was depicted in Figure 2, which shows its brittle nature. Therefore, in this case, the tensile strength is coincident with tensile stress at break. Figure 3 shows the values of tensile strength of PHB, before and after each extrusion cycle. It can be observed that the tensile stress at break decreased from 32.1 MPa to 13.4 MPa after three extrusion cycles. At the 3rd cycle, the tensile stress at break had the same order of magnitude of the tensile strength of LDPE^[45]. However, the elongation at break of these two polymers is very distinct and the tactile sensation of PHB at the 3rd cycle is like a brittle material, which hindered additional extrusion cycles for further characterization of samples.

According to Pillin et al.^[5], a similar decrease in tensile strength values was observed only at the 6th injection cycle for PLA. Nevertheless, the properties of PLA stay useful,

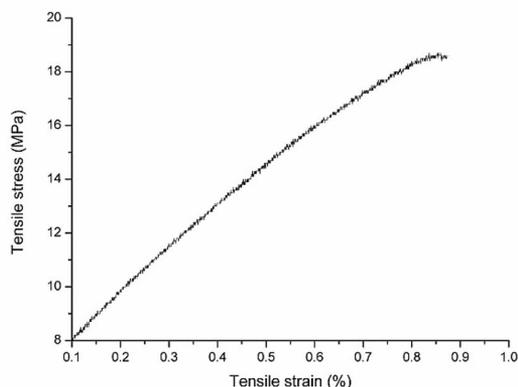


Figure 2. Representative tensile stress-strain curve of virgin PHB determined at 1 mm.min⁻¹ by using a universal machine Shimadzu AG-X 10kN model, based on the ISO standard 527- 2. The test-specimens, type 5B, were prepared by laser cutting from films prepared by compression molding.

i.e., above about 10 MPa, until the 7th cycle, the maximum number of cycles evaluated.

The color change of PHB from an off-white powder to opaque brown color was observed after first extrusion, as reported in the literature^[46,47]. Such behavior is accounted for PHB chromophoric carbonyl groups.

The strong decrease in tensile strength is probably ascribed to a reduction in the molecular weight of PHB due to chain scission reactions caused by thermal degradation^[15,20,31] during extrusion cycles. It is well established that the former properties are strongly affected by chain scission, since the broken chains are confined in the amorphous regions between the lamellae, where tie molecules, which are responsible for the mechanical integrity of semicrystalline polymers, are located^[48].

The hypothesis of mechanical properties decrease with molecular weight was in good agreement with the results achieved by Sadi et al.^[47] and Renstad et al.^[49]. In both works, the tensile strength at break for PHB and (poly-3-hydroxy butyrate-co-valerate) (PHBV), respectively, decreased with molecular weight depression. Nevertheless, none of these studies have determined until how many extrusion cycles the mechanical properties of PHB still useful and the rate that decay in the mechanical properties with extrusion cycles occurs. Kendall^[50], for example, in its life cycle assessment for the production of PHB from material recovery facilities considers that there is no current technology for PHB mechanical recycling, but in this study results show that it is possible to recycle PHB up to three extrusion cycles without any additive to inhibit its degradation or improve its properties. For conventional plastics, it is known that during thermomechanical recycling^[51-53], mechanical properties decrease with increasing multiple extrusion or injection molding cycles. This trend depends upon the type and chemical nature of the polymer. Nevertheless, blends of recycled polymers with virgin ones, reprocessing with stabilizers and incorporation of reinforcing fillers are alternatives to improve recycled plastics properties^[54-57].

Furthermore, changes in mechanical properties could be also attributed to changes in the structure and stability of crystalline state or rearrangement of interlamellar amorphous state^[44,58-60]. Nevertheless, changes in molecular weight or crystalline and amorphous morphologies are beyond the scope of this study.

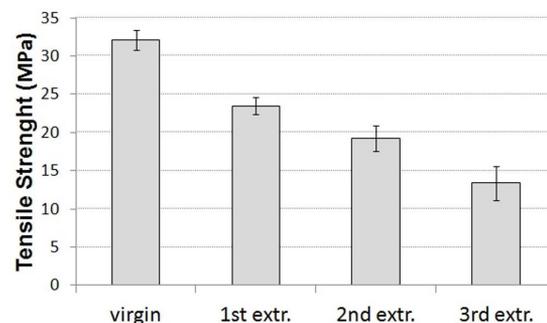


Figure 3. Results of tensile strength for PHB before and after each extrusion cycle.

3.2 Fourier transform infrared (FTIR) spectroscopy

The original chemical structure of PHB consists of molecules terminated by a hydroxyl and a carboxyl group. The hydroxyl and carboxyl end groups are observed at approximately 3600 cm^{-1} and 1720 cm^{-1} , respectively. Other characteristic PHB vibrations appear at around 1277 cm^{-1} and 970 cm^{-1} . The peak at 1277 cm^{-1} denotes the -O-C- group and at 970 cm^{-1} is assigned to bending vibrations of olefinic -C-H ^[61,62].

As the thermal degradation proceeds, it incorporates vinyl (crotonate) ester and carboxyl groups end groups in PHB structure^[20,30,31,41]. Therefore, a gradual increase in crotonate ester groups with extrusions paths can be expected, as well as a decrease in hydroxyl groups present in the original polymer. The absorption band assigned to stretching vibrations of double carbon/carbon bond, -C=C- , is expected to appear at around 1660 cm^{-1} ^[63].

FTIR analyses of PHB samples during extrusion cycles are shown in Figure 4, which presents the spectra of virgin PHB and PHB after each extrusion cycle.

The presence of absorption bands associated to the formation of new chemical groups due to degradation mechanisms of polymer was not noticed. According to Yu et al.^[64], the band at $1700\text{-}1720\text{ cm}^{-1}$, assigned to the carbonyl absorption band in the infrared spectra, is shifted to 1654 cm^{-1} when conjugated with vinyl end groups. Nevertheless, no shift can be observed for this band (Figure 5), corroborating the results of Yu et al.^[44] that observed no difference in infrared absorption of PHB film surface even after up to 40 wt% of the PHB film submitted to alkaline hydrolysis had been decomposed into crotonic acid and 3-hydrobutyric acid. In relation to the intensity of absorption band at 1720 cm^{-1} , nothing can be commented, since absorption intensity in ATR/FTIR spectroscopy depends largely on the quality of contact between sample and crystal^[65].

3.3 Thermogravimetric analysis (TGA)

Table 1 shows the values of temperature at the peak of the DTG curve (T_{max}) and the temperature at which the sample loss 10% of its initial weight ($T_{10\%}$). A peak on a DTG curve characterizes the temperature at the highest rate of thermal degradation. Figure 6 depicts the TGA curves of PHB before and after multiple extrusion cycles.

According to the literature^[20,30,31,41], as PHB degradation proceeds, an ester chain with an unsaturated ester as end group, and an ester chain with a carboxylic acid as end group are formed. Each of these two types of ester may react at a distinct rate. However, COOH and COOR groups have very similar inductive effects^[66], such that any structural changes suffered by PHB during extrusion cycles were not enough to change the thermal behavior of PHB. The TGA curves are all superposed and only a slight shift between them at the beginning of the curve could be verified (Figure 6).

No mass loss was observed until about $225\text{ }^{\circ}\text{C}$ and the temperature at DTG peak (T_{max}) was about $300\text{ }^{\circ}\text{C}$. The thermal decomposition of PHB takes place within a narrow temperature range, i. e., $235\text{ }\sim\text{ }315\text{ }^{\circ}\text{C}$. For all samples, the residual weight is lower than 0.5 wt%. Each TGA curve indicates a single step degradation, which means that the

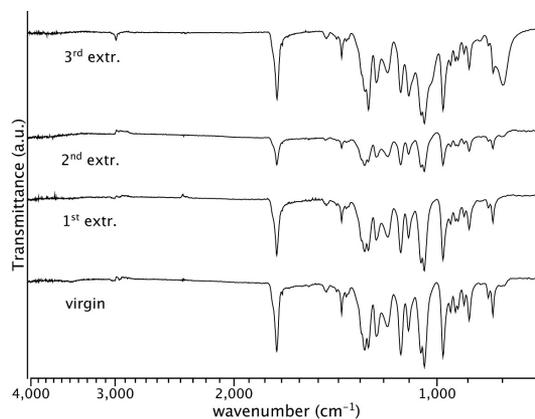


Figure 4. FTIR spectra of PHB as a function of each extrusion cycle.

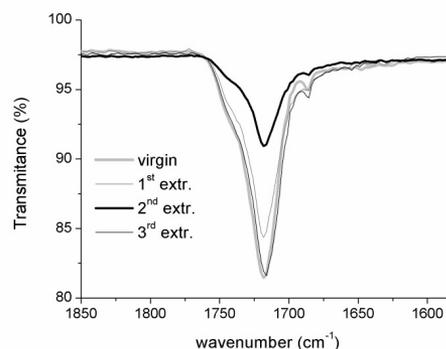


Figure 5. FTIR spectra in stretching region of -C=O of PHB before and after each extrusion cycle.

Table 1. Temperature data from TGA curves of virgin and reprocessed PHB.

Extrusion cycle	$T_{10\%}$ ($^{\circ}\text{C}$)*	T_{max} ($^{\circ}\text{C}$)**
0	271.0	297.2
1 st	271.0	297.1
2 nd	271.1	299.5
3 rd	270.7	297.4

* $T_{10\%}$ - temperature at 10 wt% of weight loss; ** T_{max} - temperature at the inflection point of the peak of DTG curve.

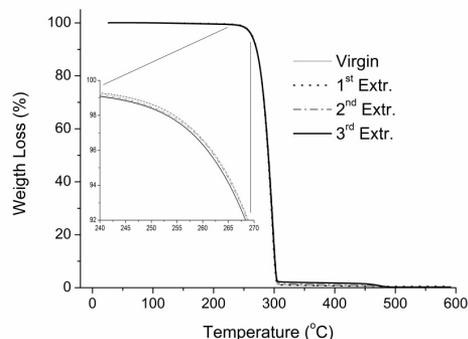


Figure 6. Thermogravimetric curves of PHB as a function of extrusion cycles.

Table 2. Thermal properties of PHB as a function of extrusion cycles.

Extrusion cycle	Xc (%)	Tm (°C)
0	57.7	174
1 st	58.8	172
2 nd	62.7	172
3 rd	62.2	172

thermal degradation of PHB polymer chains occurs by only one mechanism^[39].

3.4 Differential scanning calorimetry (DSC)

The results of the crystallinity degree (Xc) and melting temperature (Tm) are shown in Table 2.

According to these results, the crystallinity degree increased from 57.7 to 62.2%, this increase was more noticeable from the first to the second extrusion cycle. This evolution of the crystallinity with the number of extrusion cycles is also likely to be ascribed to a gradual decrease of the molecular weight of PHB which enhances the mobility and increases crystallization during the cooling step. This phenomenon is also known as chemicrystallization process^[47]. Corroborating with this hypothesis, there is the tensile strength results that conversely decreased with extrusion cycles, indicating that the increase in crystallinity does not occur with the increase of tie molecules, responsible for transferring stress between two crystalline lamellae. The same behavior was observed for PLA at multiple injections cycle^[5]. Furthermore, contributions of physical processes related to constraints imposed by amorphous chains^[60] due to progressive crystallization process of PHB can be disregarded because each measurement was carried out at the same aging time.

The melting temperature decreases slightly at the first extrusion cycle and remains constant for further extrusion cycles. This modification in melting temperature reflects the formation of less perfect crystalline regions, which corroborates with the possibility of molecular weight reduction^[25].

4. Conclusions

Along multiple extrusion cycles, PHB suffered several changes such as, decrease in mechanical properties and increase in the degree of crystallinity. According to these results, a loss in tensile strength at break of PHB above 50% was observed at the third extrusion cycle. Nevertheless, that decrement in mechanical properties was significant at the second cycle, i.e., ~40%. Also an increase in crystallinity degree was noticed mainly from the first to the second extrusion cycle, which probably could be associated to chemicrystallization process. FTIR results did not show any significant changes in polymeric structures associated to the formation of new chemical groups. Similarly, the thermal stability of PHB along processing cycles exhibited only a trend to decrease the thermal stability with extrusions paths, as evidenced by TGA curves. It is worth to note that the recyclability potential explored in this work refers to property retention up to three extrusion cycles under extreme recycling conditions (100% recycling with no added virgin polymer

and no additive or reinforcement). Therefore, improvement in PHB recyclability can be achieved by mixtures with virgin PHB, or incorporation of stabilizers and/or chain extenders to control its degradation during reprocessing.

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