Characterization of the BFO-BZN-based electroceramic composite for application as DRA

(Caracterização do compósito eletrocerâmico baseado em BFO-BZN para aplicação como DRA)

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Abstract

The study and development of ceramic composites are important because of the properties that these materials can provide, such as high dielectric constant and low dielectric loss in the RF and microwave range. Such characteristics make this type of material appropriate to several segments, such as in the telecommunication sector, especially in dielectric resonator antenna (DRA). Ceramic composites provide new materials with a range of properties that can be controlled through the phases to meet the specifications of a given application. This study aimed to synthesize and characterize the composite based on hexaferrite (BFO) and ceramics based on bismuth (BZN), aiming application as DRA. The composites were characterized by FTIR, XRD, and SEM. The composites presented a compact and heterogeneous microstructure, indicating that the sintering at 1000 °C/150 min was adequate for obtaining the ceramic composites; besides, BFO-BZNβ composite was shown to be less porous than the composite BFO-BZNα.

Keywords: ceramic composites, hexaferrite, BZN, DRA.

Resumo

O estudo e desenvolvimento de compósitos cerâmicos possui elevada importância devido às propriedades que esses materiais podem fornecer, tais como elevada constante dielétrica e baixa perda dielétrica na faixa de RF e micro-ondas. Tais características tornam esse tipo de material aplicável a diversos segmentos, como no setor de telecomunicações, em especial em antena dielétrica ressonadora (DRA). Compósitos cerâmicos fornecem novos materiais com uma gama de propriedades que podem ser controladas através das fases para atender as especificações de uma determinada aplicação. Esse estudo teve como objetivo sintetizar e caracterizar o compósito baseado em hexaferrita (BFO) e cerâmicas à base de bismuto (BZN) visando aplicação como DRA. Os compósitos foram caracterizados por FTIR, DRX e MEV. Os compósitos apresentaram microestrutura compacta e heterogênea, indicando que a sinterização em 1000 °C/150 min foi adequada para obtenção dos compósitos cerâmicos, sendo o que compósito BFO-BZNβ se mostrou menos poroso que o compósito BFO-BZNα.

Palavras-chave: compósitos cerâmicos, hexaferrita, BZN, DRA.

INTRODUCTION

The rapid growth of satellite and mobile radio communications has led to a requirement for narrowband, frequency-stable filters and oscillators. Selectivity and stability are necessary to ensure that signals are confined to closely defined allotted frequency bands and to prevent the intrusion of unwanted signals which would interfere with the satisfactory performance of the system. Antennae are also critical components of any wireless communications system. The need for compactness in satellite and hand-held mobile systems is self-evident [1]. The solution to providing stable filters and oscillators in the past lay in bulky coaxial and cavity resonators fabricated from the temperature-stable

metal alloy Invar. The dielectric resonator (DR) offers a means of miniaturizing the device. In its simplest form a DR is a cylinder of ceramic of relative permittivity ε_r sufficiently high for standing electromagnetic wave to be sustained within its volume because of reflection at the dielectric-air interface [1].

The development of ceramic composites for wireless transmission systems applications has been a subject of research and discussions in technological institutes, universities, and companies. The increasing demand for solutions for this branch of the telecommunications sector, which involves low energy consumption, minimization of component dimensions and cost reduction, has led to an interest in ceramic composites [2]. Ceramic composites are attractive for telecommunications because of the flexibility of features that can be obtained by the mixture of two or more phases, providing new materials with a wide

range of properties (mechanical, magnetic, optical and dielectric properties) that can be controlled through phase composition to meet the desired specifications necessary for a particular application. There are several applications such as capacitors, substrates for encapsulation of electronic circuits, antennas, sensors, high voltage insulation, and fuel cells [3, 4].

The increasing development of composites associated with the propagation of signals in the microwave range allows the use of these materials in wireless applications and in the design of antennas. For the construction of these composites, the ferrites are important because of their applications in telecommunications and electronic devices, while the bismuth-based ceramics are suitable for the application of antennas due to their relatively high dielectric constant and low dielectric loss in the RF and microwave range [2, 5, 6]. A combined study of both the crystal structure and the electrophysical properties of new compounds and solid solutions is necessary for the development of new ceramic materials. A refinement of stoichiometric compositions and homogeneity regions of new materials is desirable [7]. The objective of this study was to prepare and characterize the electroceramic composite based on hexaferrite and ceramics based on bismuth, aiming application as a dielectric resonator antenna (DRA).

EXPERIMENTAL

Synthesis of BFO-BZN electroceramic composites: the oxides Fe₂O₃, Bi₂O₃, ZnO, Nb₂O₅, and carbonate BaCO₃ used in the synthesis of the BFO and BZN phases were analytical grade reagents with high purity (Sigma-Aldrich). The BFO and BZN phases were prepared separately, where the precursor reactants were weighed in stoichiometric amounts, milled in a planetary mill (Fritsch, Pulverisette 6) at a speed of 370 rpm, using 10 mm diameter stainless steel beads. After obtaining the ceramic powders, they were calcined in a muffle furnace (Jung, LF0614) at 1000 °C/24 h (BaFe₁₂O₁₉ - BFO) or 700 °C/2 h (Bi_{1.5}ZnNb_{1.5}O₇ - α-BZN,

and $Bi_2Zn_{2/3}Nb_{4/3}O_7$ - β -BZN) in ar. The reactions that occurred during calcination were [8, 9]:

$$BaCO_3(s) + 6Fe_2O_3(s) \rightarrow BaFe_{12}O_{10}(s) + CO_2(g)$$
 (A)

$$0.75Bi_2O_3(s)+ZnO(s)+0.75Nb_2O_5(s) \rightarrow Bi_1 {}_{S}ZnNb_1 {}_{S}O_2(s)$$
 (B)

$$Bi_2O_3(s)+0.67ZnO(s)+1.3Nb_2O_5(s) \rightarrow Bi_2Zn_{0.67}Nb_{1.33}O_7(s)$$
 (C)

The obtained BFO and BZN ceramic powders were weighed stoichiometrically, milled in a planetary mill (Fritsch, Pulverisette 6) for 10 min. Then the mixture of these materials was uniaxially disc-shaped, sintered at 1000 °C for 150 min. The samples were named according to the concentration of hexaferrite $BaFe_{12}O_{19}$ (BFO) present in the composites: $(BFO)_y+(\alpha-BZN)_{1-y}$ and $(BFO)_y+(\beta-BZN)_{1-y}$ (Table I).

Characterization of BFO-BZN electroceramic composites. Fourier-transform infrared (FTIR) spectroscopy: the analyzes were performed in an FTIR spectrometer (Bruker, Vertex 70v) using the attenuated total reflectance (ATR) accessory. Spectra were obtained in the transmission mode with KBr pellets in the range of 130 to 4000 cm⁻¹ with a resolution of 4 cm⁻¹. X-ray diffraction (XRD): the diffractograms of the sintered discs at 1000 °C/50 min of the ceramic composites were obtained in a diffractometer (Rigaku, Dmax-B), configured in a Bragg-Brentano type geometry, using CuKα radiation (40 kV and 25 mA, λ =0.15442 nm). The angular range in 2 θ was 20°-80° with a velocity of 0.5 °/min. Scanning electron microscopy (SEM): the analyzes to evaluate the morphology of the ceramic composites were performed in a scanning electron microscope (Tecscan, Vega II XMU) operating at 5 mA and 50 kV. The sintered samples were bonded onto a metal plate with silver conductive paint (Joint Metal, PC-200) and coated with a gold layer (Bal-Tec, MED 020), approximately 30 nm thickness, for SEM analysis.

Table I - Nomenclature of composite samples $(BaFe_{12}O_{19})_y + (Bi_{1.5}ZnNb_{1.5}O_7)_{1.y}$ and $(BaFe_{12}O_{19})_y + (Bi_2Zn_{2/3}Nb_{4/3}O_7)_{1.y}$. [Table I - Nomenclature das amostras dos compósitos $(BaFe_{12}O_{19})_y + (Bi_{1.5}ZnNb_{1.5}O_7)_{1.y}$ e $(BaFe_{12}O_{19})_y + (Bi_2Zn_{2/3}Nb_{4/3}O_7)_{1.y}$.]

Sample	BaFe ₁₂ O ₁₉ - BFO (%)	Nomenclature		
	0	BZNα		
$(BaFe_{12}O_{19})_{0.25} + (Bi_{1.5}ZnNb_{1.5}O_7)_{0.75}$	25	BZNα25		
$(BaFe_{12}O_{19})_{0.50} + (Bi_{1.5}ZnNb_{1.5}O_{7})_{0.50}$	50	BZNα50		
$(BaFe_{12}O_{19})_{0.75} + (Bi_{1.5}ZnNb_{1.5}O_{7})_{0.25}$	75	BZNα75		
${\rm Bi}_{2}{\rm Zn}_{0.67}{\rm Nb}_{1.33}{\rm O}_{7}$	0	BZNβ		
$(BaFe_{12}O_{19})_{0.25} + (Bi_2Zn_{0.67}Nb_{1.33}O_7)_{0.75}$	25	BZNβ25		
$(BaFe_{12}O_{19})_{0.50} + (Bi_2Zn_{0.67}Nb_{1.33}O_7)_{0.50}$	50	BZNβ50		
$(BaFe_{12}O_{19})_{0.75} + (Bi_2Zn_{0.67}Nb_{1.33}O_7)_{0.25}$	75	BZNβ75		
BaFe ₁₂ O ₁₉	100	BFO		

RESULTS AND DISCUSSION

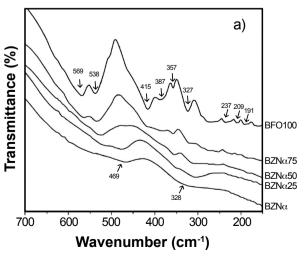
Fourier-transform infrared (FTIR) spectroscopy: the FTIR spectra of the BFO-BZNα and BFO-BZNβ ceramic composites are shown in Figs. 1a and 1b, respectively. Although hexaferrites are well-known, few studies have been reported on vibrational spectroscopy of barium hexaferrite (BaFe₁₂O₁₀) [10], because ionic materials such as Fe³⁺ oxide have the active modes in the infrared with vibrations of the crystalline lattice involving the participation of all atoms. In addition, it is important to note that the absorption frequencies, as well as the intensity of the bands in the FTIR, may vary as a function of the particle size, shape, and state of aggregation. It was observed that the frequencies, as well as band intensities, varied significantly as a function of particle size and/or volume of the BaFe₁₂O₁₀ crystallite fraction in the glass [11]. The bands located at ~237 and ~327 cm⁻¹ in the spectrum of the BFO sample can be attributed to the vibrations of the oxygen ions of the spinel block (block S) [12], since the two modes associated with the vibration of the spinel-block oxygen ions are expected in the 300-100 cm⁻¹ range. The band located at ~387 cm⁻¹ was attributed to the angular deformation of the Fe-O bond in the tetrahedron, and that located at ~415 cm⁻¹ was attributed to the stretching of the Fe-O bond in the octahedrons, and the band at 538 cm⁻¹ was attributed to the angular deformation of the Ba-O bond, thus indicating the formation of the hexaferrite BaFe₁₂O₁₉ (BFO) [13-17]. As can be seen in Fig. 1, the FTIR spectra of the samples BZN α e BZN β , as well as the composites, showed no significant differences. The absorption bands observed at 469 and 328 cm⁻¹ were attributed to the stretching of the metal-oxygen bond in the sample BZN α , and the bands at 601, 515, 447 and 328 cm⁻¹ were attributed to the stretching of the metal-oxygen bond in the sample BZNβ [18-21]. Pyrochlore oxides with different cations at site A or B may appear as distinct configurations because the exact positions of the atoms may change slightly [22]. The absorption bands at about 300 and 400 cm⁻¹ are

shown as A-O elongation vibration modes in the AO_6O_2 polyhedron [23].

X-ray diffraction (XRD): Figs. 2a and 2b show the XRD patterns of the ceramic composites BFO-BZNa and BFO-BZNβ, respectively, sintered at 1000 °C/150 min. The XRD data of the BFO sample showed a predominance of the magnetoplumbite structure BaFe₁₂O₁₉, with the P6/mmc space group, hexagonal symmetry, as evidenced by the highest intensities of peaks between 30° and 40° (hkl= 107) and 114). All peaks were in-line with the diffraction pattern ICSD PDF 84-0757. XRD pattern of BZNα sample showed the formation of the α-BZN (Bi_{1.5}ZnNb_{1.5}O₇) phase with space group Fd3m, $\alpha=\beta=\gamma=90^{\circ}$, a=b=c=10.557 Å, density of 7.044 g/cm³ and unit cell volume of 1176.6 Å³, which conformed to the standard ICSD PDF 00-052-1770, and also the formation of a small amount of the phases BiNbO. (ICSD PDF 00-016-0295) and ZnO (ICSD PDF 00-003-0752) [8]. These remaining phases were precursor phases of α -BZN, according to the reaction indicated in Eq. D [24]. That was completed at around 800 °C for a time of 300 min. As the reaction is diffusional, at higher temperatures, smaller reaction times are required, therefore, at 1000 ° C an almost pure α-BZN phase was obtained, even for short sintering time [7].

$$BiNbO_4 + ZnO \rightarrow \alpha - BZN$$
 (D)

XRD pattern of BZNβ sample showed the formation of β-BZN (Bi₂Zn_{2/3}Nb_{4/3}O₇) phase with the C2/c space group, α = γ =90.0°, β =101.256°, a=13.119 Å, b=7.671 Å, c=12.165 Å, density of 7.719 g/cm³, and volume of the unit cell of 1200.7 ų, which were in accordance with the ICSD standard PDF 00-052-0141, and two remaining phases, Bi₅Nb₃O₁₅ (ICSD PDF 00-016-0293) and BiNbO₄ (ICSD PDF 01-071-1518), following the reaction path shown in Eq. E [8]. At 700 °C the time required for complete formation of β -BZN is quite high, partially observing its formation and the presence of remaining phases; with increasing



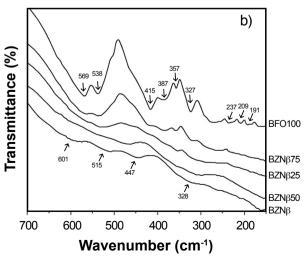


Figure 1: FTIR spectra of BFO-BZNα (a) and BFO-BZNβ (b) ceramic composites sintered at 1000 °C/150 min. [Figura 1: Espectros de FTIR dos compósitos cerâmicos BFO-BZNα (a) e BFO-BZNβ (b) sinterizados a 1000 °C/150 min.]

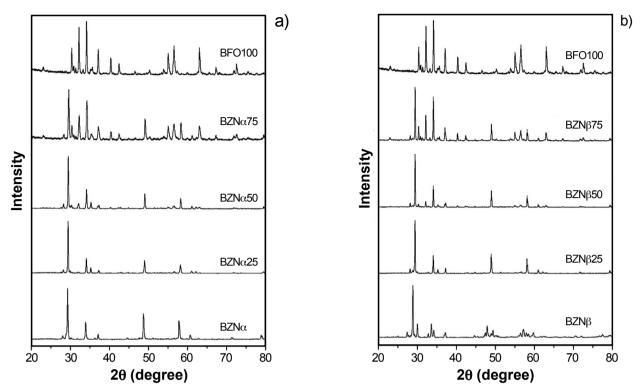


Figure 2: XRD patterns of the BFO-BZNα (a) and BFO-BZNβ (b) ceramic composites sintered at 1000 °C/150 min. [Figura 2: Padrões de DRX dos compósitos cerâmicos BFO-BZNα (a) e BFO-BZNβ (b) sinterizados a 1000 °C/150 min.]

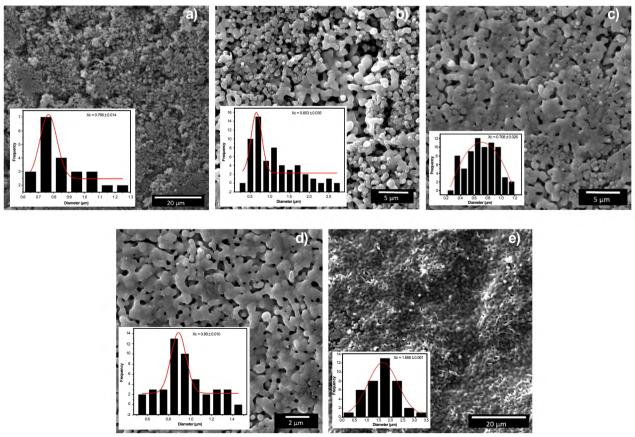


Figure 3: SEM micrographs of the BFO-BZN α ceramic composites sintered at 1000 °C/150 min: a) BFO; b) BZN α 75; c) BZN α 50; d) BZN α 25; e) BZN α 8.

[Figura 3: Micrografias de MEV dos compósitos cerâmicos BFO-BZNa sinterizados a 1000 °C/150 min: a) BFO; b) BZNa75; c) BZNa50; d) BZNa25; e) BZNa.]

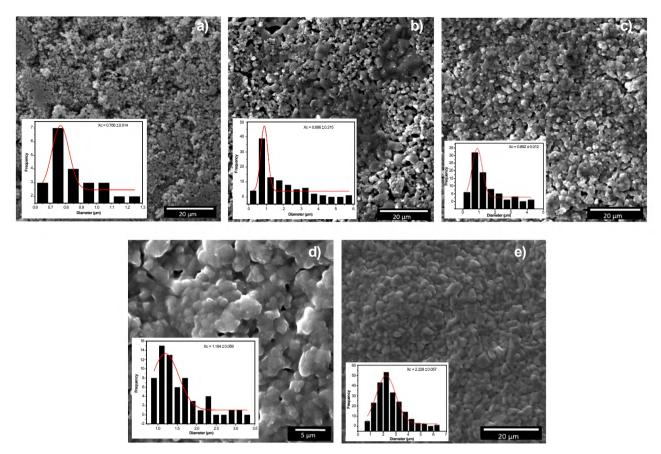


Figure 4: SEM micrographs of the BFO-BZN β ceramic composite sintered at 1000 °C/150 min: a) BFO; b) BZN β 75; c) BZN β 50; d) BZN β 25; e) BZN β 8.

[Figura 4: Micrografias de MEV dos compósitos cerâmicos BFO-BZNβ sinterizados a 1000 °C/150 min: a) BFO; b) BZNβ75; c) BZNβ50; d) BZNβ25; e) BZNβ.]

Table II - Elemental composition (at%) of composites BFO-BZNα and BFO-BZNβ. [Tabela II - Composição elementar (% atômica) para os compósitos BFO-BZNα e BFO-BZNβ.]

Element	BFO	BZNα75	BZNα50	BZNα25	BZNα	BZNβ75	BZNβ50	BZNβ25	BZNβ
0	9.1	15.7	27.6	32.2	33.2	15.9	29.0	33.8	33.4
Zn	-	3.0	4.3	5.7	6.7	1.6	3.2	0.95	4.6
Nb	-	7.1	11.1	16.8	19.0	6.1	5.6	14.1	16.5
Bi	-	15.5	23.5	32.3	35.7	17.6	18.3	15.6	41.9
Ba	14.1	8.0	4.6	2.5	-	9.0	24.5	39.0	-
Fe	71.3	43.2	21.9	9.3	-	45.2	10.8	2.1	-

temperature, there is an increase in the diffusion rate and consequent increase in the reaction rate and reduction in the reaction time, generating higher amounts of $\beta\text{-BZN}$ at $1000~^\circ\text{C}$ in relation to the sample calcined at $700~^\circ\text{C}$ [8]. The formation of $\beta\text{-BZN}$ at $1000~^\circ\text{C}$ for 2~h of treatment was almost complete, with some X-ray diffraction peaks characteristic of other remaining phases of the reaction mechanism, however, refinement indicated 100% of $\beta\text{-BZN}$, establishing that at this temperature and treatment time an appreciable amount of this phase was obtained [8].

$$Bi_sNb_3O_{1s} + BiNbO_4 + 2ZnO \rightarrow 3\beta - BZN$$
 (E)

Scanning electron microscopy (SEM): Figs. 3 and 4 show the obtained SEM images for the composites BFO-BZN α and BFO-BZN β , respectively, and the grain size distribution for all studied samples. As can be seen in Fig. 3, the microstructures were formed by clusters of grains, originated from the sintering of the nanometer-sized particles during the heat treatment. The samples exhibited a dense microstructure showing grains and agglomerates of grains of various sizes, as well as a certain degree of porosity. These porous microstructures were derived from the synthesized powders having an unfavorable particle size distribution and aggregates (Figs. 3a and 3e). It was

also observed a heterogeneous microstructure with grains larger than 0.6 µm (generated from the coalescence of the particles of the agglomerated groups) mixed with smaller grains. The grain size distribution histograms (inserts in Fig. 3) showed that the mean grain size was between about 0.7 and 0.9 µm for the BFO-BZNa ceramic composites. The BFO and BZNα samples had an average grain size of ~0.77 and ~1.7 µm, respectively. The microstructures of the BFO-BZNβ composites (Fig. 4) were also formed by agglomerated grains originating from the sintering of nanosized particles during the heat treatment. The samples exhibited a dense microstructure, with elongated and hexagonal grains, of different sizes (insets in Fig. 4). A heterogeneous microstructure with grains larger than 0.7 µm (generated from the coalescence of the particles of the agglomerated groups) mixed with smaller grains was also observed. The grain size distribution histograms (insets in Fig. 4) showed that the mean particle size was between about 0.9 and 1.2 µm for the BFO-BZNβ ceramic composites. The BFO and BZNβ samples had a mean particle size of ~ 0.77 and $\sim 2.3 \mu m$, respectively. Compared to BFO-BZNa composites, BFO-BZNβ composites exhibited lower porosity. The results of the EDS (energy dispersive spectroscopy) analyzes for the BFO-BZNα and BFO-BZNβ composites are shown in Table II.

CONCLUSIONS

The synthesis of the BFO-BZN α and BFO-BZN β composites by the ceramic method was satisfactory, since the microstructures of the composites presented grains with sizes between 0.6-0.9 μ m and 0.9-1.2 μ m, respectively, close to the grain sizes obtained by other synthesis methods. The composites presented a compact and heterogeneous microstructure, indicating that the temperature used for sintering (1000 °C/150 min) was adequate for obtaining the ceramic composites; the composite BFO-BZN β was less porous than the composite BFO-BZN α . The XRD patterns of samples BZN α and BZN β showed the presence of second-phases, indicating that the calcination at 700 °C/2 h was insufficient to obtain the pure phases of these materials.

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(Rec. 19/05/2019, Rev. 25/06/2019, Ac. 17/07/2019)

