

# THERMAL DECOMPOSITION OF TORREFIED AND CARBONIZED BRIQUETTES OF RESIDUES FROM COFFEE GRAIN PROCESSING

## Decomposição térmica de briquetes torreficados e carbonizados de resíduos do processamento dos grãos de café

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### ABSTRACT

The use of biomass has been recognized as a potential renewable energy and an alternative substitute that contributes to the decrease of fossil fuels consumption. Therefore, this research aimed to analyze the thermal behavior of briquettes made of residues from coffee grain processing in different conditions: *in natura*, torrefied and carbonized. *Eucalyptus* sawdust was used for comparison. The briquettes were carbonized considering final temperature of 450° C (kept for 30 min). The briquettes torrefaction was performed in an electric oven (muffle) using two heating rates until 250° C (kept 60 min). The thermal-gravimetric analysis was made in nitrogen atmosphere until the temperature of 600° C. The contents of fixed carbon and volatile matter of the fuels were determined. The carbonized briquette of residues from coffee grain processing presented higher stability and low thermal decomposition. It was observed a low influence of torrefaction heating rate under thermal properties of briquettes, and fixed carbon and volatile matter content. Regarding the raw biomass, lower total mass loss was observed for the residues from coffee grain processing when compared to *Eucalyptus* sawdust. The carbonized and torrefied briquettes presented higher hydrophobicity than raw briquettes.

**Index-terms:** Solid biofuels, residual biomass, coffee plantations, stability.

### RESUMO

O uso da biomassa tem sido reconhecido como uma energia potencial renovável e um substituto alternativo que contribua para a redução do consumo de combustíveis fósseis. Portanto, objetivou-se analisar o comportamento térmico de briquetes de resíduos do processamento dos grãos de café, em diferentes formas: *in natura*, torreficados e carbonizados. Utilizou-se a serragem de *Eucalyptus* como parâmetro de comparação. Os briquetes foram carbonizados considerando a temperatura final de 450° C (mantida por 30 min). A torrefação dos briquetes foi realizada em uma mufla em duas taxas de aquecimento até 250° C (mantida por 60 min). Realizou-se a análise termogravimétrica em atmosfera de nitrogênio até a temperatura de 600° C. Determinaram-se os teores de carbono fixo e materiais voláteis dos combustíveis. O briquete carbonizado dos resíduos do processamento dos grãos de café apresentou a maior estabilidade e baixa decomposição térmica. Observou-se baixa influência da taxa de aquecimento de torrefação nas propriedades térmicas dos briquetes e nos teores de carbono fixo e materiais voláteis. Quanto às biomassas *in natura* observou-se menor perda de massa total para os resíduos do processamento dos grãos de café em comparação a serragem de eucalipto. Os briquetes carbonizados e torreficados apresentaram caráter mais hidrofóbico em relação ao briquete *in natura*.

**Termos para indexação:** Biocombustíveis sólidos, biomassa residual, cafeicultura, estabilidade.

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### INTRODUCTION

The use of biomass has been recognized as a potential renewable energy and an alternative substitute that contributes to the decrease of fossil fuels consumption (SHEN; GU, 2009; KIM; EOM; WADA, 2010; PROTÁSIO et al., 2013). In this context, Brazil has advanced in relation to the use of clean renewable energy due to its potential on agricultural and forest cultures. Almost 46% of Brazilian energetic matrix is derived from renewable resources, 14% corresponding to hydropower

and 32% related to several types of biomass and other renewable energies (BRASIL, 2011).

Among agricultural residues, the bark and parchment of coffee derived from the fruit processing may be highlighted as a raw material of high energetic potential, since it is produced in large scale in Brazil, the largest coffee producer of the world; in 2012 this country must harvest from 48.97 to 52.27 millions of bags of processed coffee (COMPANHIA NACIONAL DE ABASTECIMENTO-CONAB, 2012). Moreover, this

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lignocellulosic residue presents chemical, physical and energetic characteristics favorable to the production of bioenergy through thermochemical processes (PAULA et al., 2011a; PAULA et al., 2011b; PROTÁSIO et al., 2011a; PROTÁSIO et al., 2011b; PROTÁSIO et al., 2012a; PROTÁSIO et al., 2012b).

This way, the residues generated by this process consist of an attractive alternative source of energy, but firstly it is necessary to improve techniques in order to solve some limitations in relation to the use of biomass *in natura*, like the high content of moisture, low energetic density (PROTÁSIO et al., 2011a), hygroscopic behavior, difficulties on storing and transporting.

Chen and Kuo (2011) suggests that some of these problems may be reduced through thermal pre-treatment of biomass, and the torrefaction is one of the methods liable to be applied. In this process the biomass *in natura* is heated to 225-300° C (PRINS; PTASINSKI; JANSSEN, 2006).

Some results found on literature confirm the efficiency of torrefaction is one of the methods liable to be applied on the improvement of some properties of biomass, like the increase of energetic density (FELFLI et al. 2005; PRINS; PTASINSKI; JANSSEN, 2006; COUHERT, SALVADOR; COMMADRÉ, 2009; YAN et al., 2009) and the proportion C/O, which results in the increase of fuel energetic value (BRIDGEMAN et al., 2008; COUHERT, SALVADOR; COMMADRÉ, 2009; YAN et al., 2009; PROTÁSIO et al., 2012a), inversion of the characteristic hygroscopic behavior for hydrophobic (DENG et al., 2009; PROTÁSIO et al., 2012a), such the torrefied fuel presents low moisture content and facility to be stored, besides significant improvement of inflammability, reactivity and milling (ARIAS et al., 2008; BRIDGEMAN et al., 2008; REPELLIN et al., 2010).

In this sense, the use of thermal analyses plays an important role on evaluating the performance of lignocellulosic material to be used on thermochemical processes. The thermal-gravimetric analysis (TGA) is an important tool on identifying degradation phases of biomass constituents and, consequently, for the analysis of torrefaction and carbonization efficiency.

Therefore, the objective of this work was to analyze the thermal behavior of briquettes made of residues from coffee grains processed *in natura*, torrefied and carbonized. Sawdust of *Eucalyptus* was used for comparisons.

## MATERIAL AND METHODS

In order to produce the briquettes, residues from coffee (*Coffea arabica* L.) grain processing, bark and

parchment of the variety Icatu IAC 3282 from EPAMIG experimental farm in the municipality of Machado, Minas Gerais state (21° 40' 42,54" S 45° 56' 31,38" W) were used. The plantation was established on 1995.

The biomass was ground in hammer mill, in which a sieve 2mm mesh was linked for granulometric reduction. It was posteriorly classified in sieves 40, 60 and 270 mesh. Compressed residual biomass contained 84% of particles with diameter longer or equal to 0.425mm, 11% with diameter between 0.425mm and 0.250mm, and 5% with diameter shorter than 0.250mm.

Compressing of residues was made in a hydraulic briquetter Lippel®, model LB 32. The biomass was previously dried at  $103 \pm 2^\circ$  C. The temperature used for compressing was  $120 \pm 5^\circ$  C and pressure equal to 15 MPa. Briquettes were produced with diameter of approximately 3 cm and 6 to 7 cm high (PAULA et al., 2011a; PROTÁSIO et al., 2011a).

Carbonization of briquettes was performed in an electric stove (muffle), using a heating rate of  $1.67^\circ$  C  $\text{min}^{-1}$ . Initial temperature was 50° C and final temperature was 450° C, kept during 30 min. Total carbonization lasted 4.5h.

Briquettes torrefaction at muffle was made with two distinct heating rates, the first of  $1.5^\circ$  C  $\text{min}^{-1}$  (rate 1) and the second of  $3.0^\circ$  C  $\text{min}^{-1}$  (rate 2), both with final temperature of 250° C kept during 60 minutes.

All analyses were performed for briquettes *in natura* (control briquette), as well as for thermally treated briquettes. *Eucalyptus* sawdust was used as parameter for comparison, which came from sawing of logs, once this wood is widely used for energy generation or, in the case of residues, for co-generation. Samples compounded by 6 repetitions for each treatment, *in natura*, torrefied and carbonized material were used for thermal-gravimetric analysis (TGA).

For TGA, the fuels of vegetal biomass were grounded to powder using the granulometric fraction that passed through the sieve 200 mesh and was retained by the sieve 270 mesh. The equipment DTG-60H SHIMADZU was used for this analysis. Samples of approximately 4 mg were submitted to a temperature gradient ranging from environment temperature to 600° C with heating rate of  $10^\circ$  C  $\text{min}^{-1}$  using nitrogen flow of 50 mL  $\text{min}^{-1}$ .

Using the first derivative of TG curve which establishes the mass loss in function of temperature, it was possible to identify the rate of mass loss by second and the characteristic peaks of biomass thermal degradation.

The immediate chemical analysis of biomass fuels was made in order to quantify the content of volatile matter and ashes, and by difference, the fixed carbon according

to ASTM D1762-84 standard (AMERICAN SOCIETY FOR TESTING MATERIALS-ASTM, 2007). Analysis of variance (ANOVA) were performed considering one entirely randomized design with 5 treatments (carbonized briquette, torrefied briquette in rate 1, torrefied briquette in rate 2, *in natura* briquette and *Eucalyptus* sawdust) and 4 repetitions. Mean were compared statistically by Tukey test at 5% of significance.

## RESULTS AND DISCUSSION

Mass loss in function of temperature (TG curve) of the analyzed fuels is shown on figure 1. It is possible to observe that carbonized briquettes obtained the highest thermal stability, thus presenting high resistance to thermal degradation.

Torrefied briquettes presented intermediate position. This result may be attributed to thermal treatment applied to briquettes which resulted on degradation of molecular components and consequently on carbon fixation.

In this case, it is possible to affirm that, during thermal treatment (torrefaction), endothermic reactions with release of water, acetic acid, methanol, carbon dioxide and other oxygenated gases predominated, which molecules came from thermal decomposition of hemicelluloses (PRINS; PTASINKSKI; JASSEN, 2006), thus resulting on carbon fixation (Figure 2). The greater thermal

decomposition of hemicelluloses is due to their amorphous and easily hydrolysable chemical structure (YANG et al., 2006; JOHN; THOMAS, 2008).

Fuels with higher contents of fixed carbon and low volatile matter tend to burn slowly (BRAND, 2010), because fixed carbon represents the fraction of fuel that burns on solid state, justifying the results observed on Figures 1 and 2. The reduction of the relation oxygen/carbon on fuels also provided an increase on resistance to thermal degradation, which is one of the objectives of torrefaction and carbonization processes (CHEN et al., 2011).

Regarding *in natura* biomass, it was observed that residues of coffee grain processing (control briquette), even starting thermal decomposition early, they presented higher resistance to thermal degradation and lower mass loss rate when compared to *Eucalyptus* sawdust (Figure 1).

Biomass volatilization and consequently thermal degradation depends on its chemical composition, as well as cellulose and lignin content (GANI; NARUSE, 2007). Protásio et al. (2012b) observed high content of insoluble lignin (31.03%) for bark and parchment of coffee grain, overcoming other lignocellulosic residues from agricultural and forestry activities, including *Eucalyptus* residual wood (25.65%).

The results found by Protásio et al. (2012b) corroborate with tendencies observed in this work, because among molecular chemical contents, lignin presented the

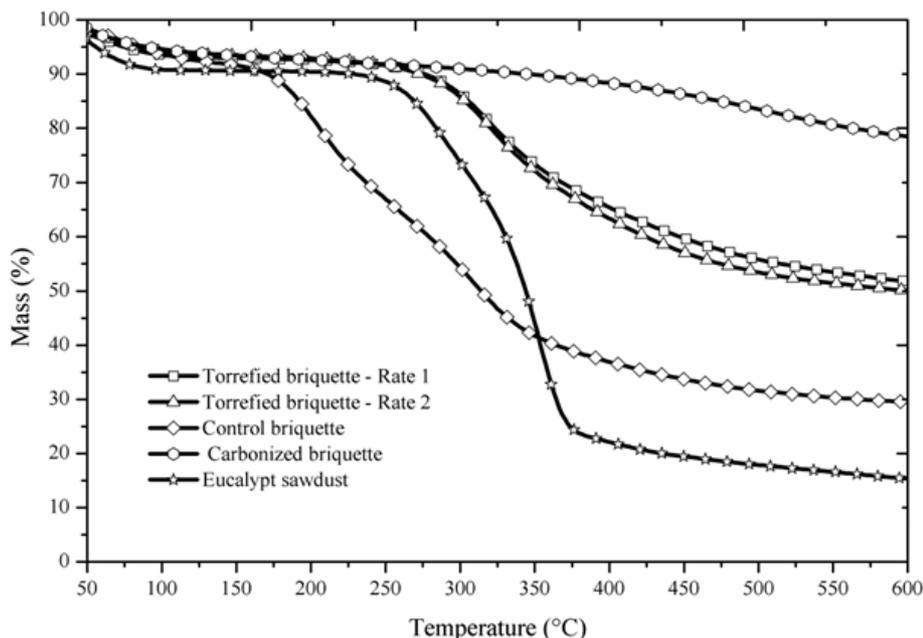


Figure 1 – Mass loss in function of temperature of the analyzed fuels.

highest thermal stability due to carbon-carbon bonds among monomeric units of phenyl-propane and consequently the stability of its aromatic matrix, besides presenting high molecular weight (SHAFIZADEH, 1985; BARTKOWIAK; ZAKRZEWSKI, 2004; SHARMA et al., 2004; YANG et al., 2006; GANI; NARUSE, 2007; JOHN; THOMAS, 2008).

There are reports on the literature related to the increase of carbon content and consequently the reduction of volatile matter content as final pyrolysis temperature increases (DEMIRBAS, 2001; TRUGILHO; SILVA, 2001; DEMIRBAS, 2004), resembling to the observed in the present work (Figure 2).

It is possible to note that carbonized briquette presented higher mean value of fixed carbon and lower volatile matter content. Torrefied briquettes at rate 1 and 2 presented similar and intermediate immediate chemical composition, and consequently the total mass loss also was similar. This result is an indicative of the low influence of heating rate used during torrefaction process on chemical and thermal properties of such fuels.

The briquette made of residues from coffee grain processing (control briquette) presented approximately 71% more fixed carbon than *Eucalyptus* sawdust, justifying the lower total mass loss (Figures 1 and 2). This result

may be attributed to the higher lignin content of residues from coffee grain processing, as reported by Protásio et al. (2012b)

Lignin contains higher carbon content than other chemical components. Thus, it is expected that the higher the lignin content, higher fixed carbon content of fuels (BARTKOWIAK; ZAKRZEWSKI, 2004; GANI; NARUSE, 2007), reinforcing the found tendencies (Figure 2).

*Eucalyptus* sawdust lost 20% more mass, considering final temperature of 600° C. Despite it is commonly used on energy generation, directly in boilers or on briquettes production (PAULA et al., 2011a; PROTÁSIO et al., 2011a), residues from sawing of *Eucalyptus* logs (sawdust) tend to burn faster, as can be observed on figures 1 and 2.

This result shows the potential of energetic use of bark and parchment of coffee grain, not only because of the high Brazilian production of this grain (CONAB, 2012), but also because of chemical, physical, energetic and thermal characteristics of this residue (PAULA et al., 2011a; PAULA et al., 2011b; PROTÁSIO et al., 2011a; PROTÁSIO et al., 2011b; PROTÁSIO et al., 2012a; PROTÁSIO et al., 2012b).

Analysing DTG curves (Figure 3), it is possible to note that *in natura* biomass presented three distinct stages of thermal degradation, it means, three peaks of mass loss.

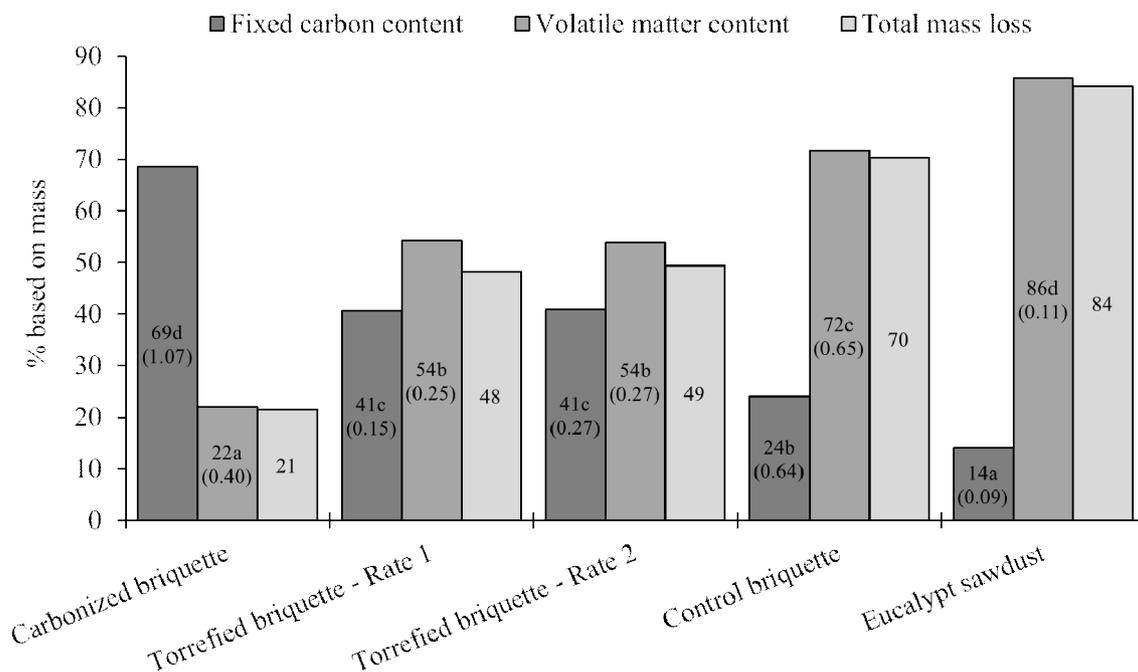


Figure 2 – Fixed carbon, volatile matter and total mass loss. Means followed by the same letter do not differ among themselves at 5% of significance by Tukey Test. Standard deviation in parentheses.

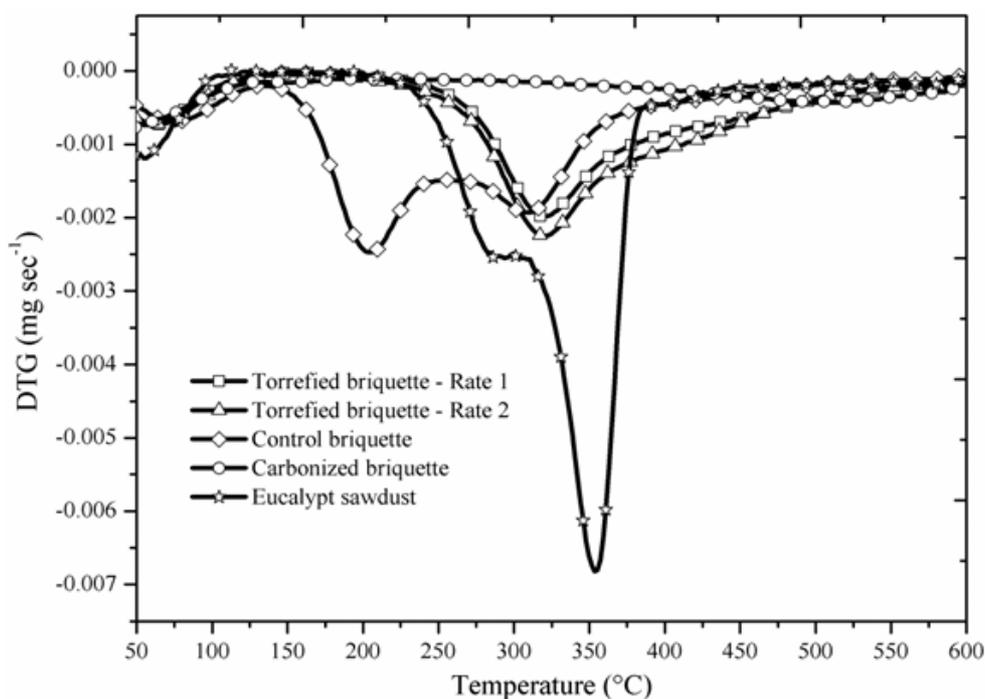


Figure 3 – DTG curves of analyzed fuels.

Thermally treated briquettes (torrefied and carbonized) presented only two stages of thermal degradation, suggesting the efficiency of thermal treatment performed.

The formation of a slight shoulder on DTG curve of *Eucalyptus* sawdust (Figure 3) is an indicative of hemicelluloses degradation, as reported by Polleto et al. (2012). The authors observed a characteristic peak of degradation of hemicelluloses present on the wood of four species in approximately 300° C, resembling to the observed in this work (288.9° C).

Hemicelluloses are degraded between 180° C and 350° C (KIM et al., 2006), cellulose between 305° C and 375° C (SHAFIZADEH, 1985) and lignin between 250 and 500° C (SHAFIZADEH, 1985; KIM et al., 2006). Therefore, during the torrefaction processes, part of the content of cellulose and lignin are preserved, justifying the presence of two typical stages of degradation.

Analyzing stage I (Table 1), relative to sample water loss, it is possible to note that *Eucalyptus* sawdust presented higher moisture in relation to the other analyzed fuels. This may be attributed to the higher hemicelluloses content, because these molecular components are the main responsible by the water absorption due to its amorphous and branched character (PRINS; PTASINKSKI; JASSEN, 2006).

In relation to fuels submitted to thermal treatment of torrefaction and carbonization, a reduction of moisture is observed (I degradation stage) (Table 1), it means, an increase of briquettes hydrophobicity occurred, what is a great advantage since water decreases considerably the caloric value of the biomass fuels. It is known that latent heat of water is approximately 2.32 MJkg<sup>-1</sup> (BRAND, 2010).

*Eucalyptus* sawdust lost 50% of mass at a temperature superior (345° C) to residues of coffee grain processing (313° C) (Figure 1), it means, forestry biomass presented thermal degradation at temperatures superior to the analyzed agricultural residue, as may be observed at the higher values obtained for onset, endset and peak temperature at stages II (in which occurs mainly degradation of hemicelluloses) and III (in which occurs only degradation of remaining hemicelluloses and celluloses). This shows that the torrefaction of briquettes from *Eucalyptus* sawdust may be technically viable resulting on high gravimetric yield in torrefied briquettes, once torrefaction is made between the temperatures 225° C and 300° C (PRINS et al., 2006).

The presence of high extractive content (components of low molecular weight) on residues of coffee grain processing (PROTÁSIO et al., 2012b) may promote the biomass inflammability at lower temperatures due to

Table 1 – Onset temperature (Ton - °C), endset temperature (Tend - °C), maximum degradation temperature (Tp - °C) and percentage of mass loss (P%)

| Fuel  | Degradation Stage I |       |      |     | Degradation Stage II |       |       |      | Degradation Stage III |       |       |      |
|-------|---------------------|-------|------|-----|----------------------|-------|-------|------|-----------------------|-------|-------|------|
|       | Ton                 | Tend  | Tp   | P%  | Ton                  | Tend  | Tp    | P%   | Ton                   | Tend  | Tp    | P%   |
| BWT   | 54.0                | 101.7 | 73.9 | 7.9 | 185.6                | 216.2 | 203.4 | 27.5 | 296.7                 | 362.4 | 310.4 | 34.9 |
| ES    | 44.7                | 46.1  | 45.3 | 9.3 | 269.5                | 290.1 | 288.9 | 12.8 | 335.1                 | 376.4 | 354.2 | 62.1 |
| BT1.5 | 44.7                | 88.1  | 56.3 | 7.0 | 282.9                | 406.0 | 318.6 | 41.0 | -                     | -     | -     | -    |
| BT3.0 | 49.5                | 94.8  | 66.1 | 6.3 | 281.2                | 407.0 | 320.3 | 43.0 | -                     | -     | -     | -    |
| CB    | 45.7                | 90.1  | 48.6 | 6.6 | 439.5                | 573.0 | 506.5 | 14.8 | -                     | -     | -     | -    |

BWT: briquette made of residues of coffee grain processing without thermal treatment; ES: *Eucalyptus* sawdust; BT1.5: briquette torrefied at 1.5° C min<sup>-1</sup>; BT3.0: briquette torrefied at 3.0 °C min<sup>-1</sup>; CB: carbonized briquette.

the higher volatility and then improve the process of thermal degradation (GRØNLI; VÁRHEGYI; DI BLASI, 2002; SHEBANI; VAN REENEN; MEINCKEN, 2008; POLLETO et al., 2012), what would justify the lower values for onset, endset and peak temperatures at stages II and III when compared to *Eucalyptus* sawdust (Table 1).

However, the mass loss of *Eucalyptus* sawdust at stage III was 78% superior to *in natura* briquette (Table 1), what may be attributed to the intense cellulose degradation (SHAFIZADEH, 1985; POLLETO et al., 2012), showing that carbonization of briquettes made of this forestry residue will result on low yield and high production of pyrolygneous liquid and not condensable gases.

Polleto et al. (2012) also observed intense cellulose degradation at 350° C studying the wood of four species, resembling to the observed in this work for *Eucalyptus* sawdust (354° C). Cellulose molecule is a long polymer formed by several glucose monomers and its crystalline regions improves the thermal stability, providing higher degradation temperature in relation to hemicelluloses (YANG et al., 2006).

Considering stage II, it is observed that thermal degradation of torrefied and carbonized briquettes started later in relation to *in natura* briquette. According to Liu et al. (2007) and Morán et al. (2008), the increase of crystalline component causes the increase of thermal stability of the sample, allowing thermal degradation to start later, as observed in this work.

It is also observed the similarity of onset, endset and peak temperature for torrefied briquettes, as well as the mass loss (Tables 1 and 2), suggesting that the heating rate of the stove had a weak influence on thermal properties of briquettes.

Carbonized briquette presented the highest maximum degradation temperature (506° C), once the pyrolysis final temperature to which it was submitted (450° C) provided the total degradation of hemicelluloses and cellulose, as well as lignin, modifying them thermally. This may be seen

through the analysis of TG and DTG of *in natura* curve, which tends to stabilize and lacks peaks of intense thermal degradation from 376 °C on, it means, from this temperature on, the biomass loss is basically attributed to the presence of residual lignin.

Therefore, the process of carbonization provided a hydrophobic character to the briquette made of residues of coffee grain processing, besides improving considerably its resistance to thermal degradation.

## CONCLUSIONS

Carbonized briquette made of residues of coffee grain processing presented the highest stability and low thermal decomposition.

It was observed a weak influence of torrefaction heating rate under stability and thermal resistance, as well as under fixed carbon and volatile matter content.

Regarding *in natura* biomass, lower total mass loss for residues from coffee grain processing was observed when compared to *Eucalyptus* sawdust. This result was attributed to the differences on chemical and immediate molecular structure of the fuels.

The results suggest an improvement of hydrophobicity of carbonized and torrefied briquettes in relation to *in natura*, and the efficiency of the pre-treatments performed.

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