Julia Dantas MAZÃO<sup>(a)</sup> Maria Tereza Hordones RIBEIRO<sup>(a)</sup> Stella Sueli Lourenço BRAGA<sup>(a)</sup> Karla ZANCOPÉ<sup>(b)</sup> Richard Bengt PRICE<sup>(c)</sup> Carlos José SOARES<sup>(a)</sup>

(•)Universidade Federal de Uberlânida – UFU, School of Dentistry, Operative Dentistry and Dental Materials Department, Uberlândia, MG, Brazil.

(b)Universidade Federal de Uberlânida – UFU, School of Dentistry, Department of Occlusion, Fixed Prosthodontic and Dental Materials, School of Dentistry, Federal University of Uberlândia, MG, Brazil.

(\*)Dalhousie University, Department of Dental Clinical Sciences, Halifax, Nova Scotia, Canada.

**Declaration of Interests:** The authors certify that they have no commercial or associative interest that represents a conflict of interest in connection with the manuscript.

**Corresponding Author:** Carlos José Soares E-mail: carlosjsoares@ufu.br

https://doi.org/10.1590/1807-3107bor-2023.vol37.0114

Submitted: Mar 4, 2023 Accepted for publication: July 12, 2023 Last revision: August 15, 2023



# Effect of thickness and shade of CAD/CAM composite on the light transmission from different light-curing units

Abstract: The thickness and shade of a restoration will affect the transmission of light from the light-curing unit (LCU). This study determined the power (mW), spectral radiant power (mW/nm), and beam profile of different LCUs through various thicknesses and shades of a CAD-CAM resin composite (BRAVA Block, FGM). Five thicknesses: 0.5; 0.75; 1.0; 1.5, and 2.0 mm, in three shades: Bleach; A2 and A3.5 of a CAD-CAM resin (n = 5). Two single-peak LCUs: EL, Elipar DeepCure-S (3M Oral Care); and OP, Optilight Max (Gnatus), and one multiple-peak LCU: VL, VALO Grand (Ultradent), were used. The LCUs were positioned touching the surface of the BRAVA Block. The power and emission spectrum were measured using a fiberoptic spectrometer attached to an integrating sphere, and the beam profiles using a laser beam profiler. The effect of the material thickness on the light attenuation coefficients was determined. VL and EL delivered more homogeneous beam profiles than OP. The type of the BRAVA Block had a significant effect on the transmitted power, and wavelengths of transmitted light (p < 0.001). There was an exponential reduction in the power and emission spectrum as the thickness of the BRAVA Block increased (p < 0.001). The light transmission through the A2 shade was least affected by the thickness (p < 0.001). The attenuation coefficient was higher for the violet light and higher for A3.5 than the A2 or Bleach shades. No violet light from the VL could be detected at the bottom of 2.0 mm of the BRAVA Block.

**Keywords:** Light; Polymerization; Computer-Aided Design; Composite Resins.

## Introduction

The use of computer-aided design and manufacturing (CAD-CAM) technology has increased exponentially in recent years.<sup>1</sup> This technology allows the prepared teeth to be scanned, the restoration designed, milled out of a CAD-CAM material and adhesively cemented to the tooth in just one appointment.<sup>2,3</sup> The two primary restorative materials used in CAD-CAM technology are ceramic and resin composite-based materials.<sup>4,5</sup> Despite having inferior mechanical and aesthetic properties

than ceramic materials,<sup>6</sup> resin composites have been proposed as a more economical alternative that can also be repaired intraorally.<sup>2,4</sup> Some CAD-CAM materials that are called hybrid ceramics, consist of a ceramic substructure surrounded by resin.<sup>3</sup> These materials are available in different shades and can be milled in various thicknesses.<sup>7</sup>

The adhesive bonding process between the tooth and the restoration is a crucial step to ensure the success of the restoration.<sup>8,9</sup> Depending on the thickness of the restorative material, two types of resin cement are recommended: either a purely light-polymerized resin cement, or a dual-cured resin cement.<sup>10-13</sup> To ensure the optimum properties of both types of cements, in both cases, sufficient light must pass through the restorative material to photocure the resin cement.<sup>14-16</sup> Using a thicker restorative material and a darker or opaque shade of the block will reduce the light transmission through the restoration. This could compromise both the bond to the tooth and the mechanical properties of the cement.<sup>17,18</sup>

The need for increasingly whiter colored and more color-stable luting cements has resulted in manufacturers using the new generation of Norrish Type I photoinitiators in their resin cement, so that they can reduce the amount of camphorquinone,<sup>19,20</sup> because camphorquinone has a bright yellow color.<sup>21</sup> Many of these alternative photoinitiators require violet light, and light manufacturers have developed light-emitting diode (LED) light curing units (LCUs) that emit both violet and blue light.<sup>22-25</sup> However, the wavelength of violet light (390–410 nm) is shorter than blue light (420–470 nm), and violet light does not penetrate through the restorative material as well as blue light.<sup>24-28</sup>

The type of LCU and the combination of the shade, opacity, and thickness of the CAD-CAM material all affect the power and wavelengths of light transmitted through the restorative material.<sup>7,29-31</sup> The irradiance value at the light tip is the radiant power (usually expressed in mW) divided by the area of the light tip (usually expressed in cm<sup>2</sup>). More expensive LCUs are often more powerful and have a greater active tip area than budget LCUs. However, the cost of LCU does not always

correlate with the irradiance delivered because the irradiance from the LCU can be increased by reducing the diameter of the light tip<sup>8,32</sup> and many budget-cost lights have a small 6 to 7 mm diameter light tip. Most studies only analyze the effect of light transmission on ceramic materials.<sup>11,12,17</sup> However, the characteristics and composition of the resin-based composite materials can also affect the beam profile of the light as it passes through the material, the wavelengths of the transmitted light, and the attenuation coefficient.<sup>7,26,33-35</sup>

Most budget-cost light-curing units usually transmit less power through different thicknesses and shades of CAD-CAM materials, which can affect the photo-activation of the resin based the luting cement.<sup>7</sup> Therefore, the purpose of this study was to evaluate the radiant power (mW), the spectral radiant power (mW/nm) of the transmitted light, and beam profiles of different LCUs through different thicknesses and shades of a glass-ceramic resin composite used for CAD-CAM restorations. The null hypothesis was that the thickness and shade of the CAD-CAM material would not affect the light transmission, wavelengths of transmitted light, beam profile or the attenuation coefficients.

## Methodology

#### Study design

Low translucency CAD/CAM blocks (BRAVA Block; FGM, Joinvile, SC, Brazil) that the manufacturer claims to be a glass-ceramic resin composite were used in 5 different thicknesses, and three shades. Two single-peak LCUs: EL (Elipar DeepCure-S; 3M Oral Care, St. Paul, USA) and OP (Optilight Max; Saevo, Ribeirão Preto, Brazil) and one multiple-peak LCU: VL (VALO Grand; Ultradent, South Jordan, USA) were used. The specifications of these LCUs are reported in Table 1. The LCUs were positioned at 0 mm from the surface of the CAD/CAM material. The power and emission spectrum were obtained using a fiberoptic spectrometer attached to an integrating sphere. The light attenuation coefficients of all three LCUs and shades were calculated for each thickness of the CAD/CAM BRAVA blocks.

| LCUs Serial number LED LCU /<br>wavelength<br>emission External Tip<br>Diameter<br>(mm) Internal Tip<br>Diameter<br>(mm) Irradiance<br>(mW/cm <sup>2</sup> ) Manufacturer   Elipar DeepCure-S 1521087817 single-peak 9.8 9.0 1500 3M Oral Care, St Paul, USA |                   |               |                                     |                                  |                                  |                        |                                |
|--|-------------------|---------------|-------------------------------------|----------------------------------|----------------------------------|------------------------|--------------------------------|
| Elipar DeepCure-S 1521087817 single-peak 9.8 9.0 1500 3M Oral Care, St Paul, USA   | LCUs              | Serial number | LED LCU /<br>wavelength<br>emission | External Tip<br>Diameter<br>(mm) | Internal Tip<br>Diameter<br>(mm) | Irradiance<br>(mW/cm²) | Manufacturer                   |
|  | Elipar DeepCure-S | 1521087817    | single-peak                         | 9.8                              | 9.0                              | 1500                   | 3M Oral Care, St Paul, USA     |
| Optilight Max 881778249 single-peak 7.9 7.0 1580 Gnatus, Ribeirão Preto, Brazil  | Optilight Max     | 881778249     | single-peak                         | 7.9                              | 7.0                              | 1580                   | Gnatus, Ribeirão Preto, Brazil |
| VALO Grand MFG3227-5 multi-peak 15.1 12.0 1150 Ultradent, South Jordan, USA  | VALO Grand        | MFG3227-5     | multi-peak                          | 15.1                             | 12.0                             | 1150                   | Ultradent, South Jordan, USA   |

Table 1. The specifications of light-curing units (LCUs) used in this study.

Table 2. The specifications of CAD-CAM resin composite blocks used in this study.

| LCUs        | Composition   | Shade         | Serial number | Manufacturer          |
|-------------|---|---------------|---------------|-----------------------|
| BRAVA Block | Methacrylate monomers, initiator, co-initiator,<br>stabilizers, silane, glass-ceramic particles,<br>silica, and pigments. | A2 LT/14L     | A2LT051220    |                       |
|             |   | Bleach LT/14L | BLLT071120    | FGM, Joinvile, Brazil |
|             |   | A3.5 LT/14L   | A35LT081220   |                       |

#### CAD-CAM resin composite preparation

The Bleach, A2, and A3.5 shades of low translucency CAD/CAM materials (Table 2) were glued to an acrylic plate with cyanoacrylate glue (Super Bonder; Loctite, Itapevi, Brazil) and sticky wax (Sticky Wax; Asfer, São Caetano do Sul, Brazil). The blocks (BRAVA Block; FGM) were sectioned into 14.5 mm X 14.5 mm slices (n = 5) that were: 0.5; 0.75; 1.0; 1.5, and 2.0 mm thick using a precision saw (IsoMet 1000; Buehler, Lake Bluff, USA) at 225 rpm under a 150g load and with copious water irrigation.

#### Total radiant power and emission spectrum

The total radiant power (mW), and spectral radiant power (mW/nm) from the 3 LCUs were determined. Five measurements of the total radiant power (mW) emitted between 350 and 550 nm and spectral radiant power (mW/nm) from the LCUs were measured using a fiber optic spectrometer (USB 4000; Ocean Insight, Orlando, USA) connected to a six-inch integrating sphere (LabSphere; North Sutton, USA). An internal calibration lamp (SCL 600; Labsphere) calibrated the system. The light transmission through the control (no interposing CAD/CAM material) and the 5 thicknesses: 0.5; 0.75; 1.0; 1.5, and 2.0 mm, for the three shades of the CAD/CAM materials was measured with the LCU tip at 0-mm through a 12 mm aperture in the integrating sphere.

#### **Beam profile**

The light beam profiles of light transmitted through the different thicknesses of glass-ceramic resin composite were measured using a laser beam profiler charge-coupled device (CCD) digital camera (Ophir-Spiricon) with a 50 mm focal length lens (SP620U; Ophir-Spiricon). The LCUs were mounted in a fixed orientation 0 mm away from the imaging screen or the CAD-CAM resin composites, facing toward the camera thus simulating all the conditions of the light transmission experiment. For the control condition, a diffusing surface 60-degree holographic diffusing screen (Edmund Optics, Barrington, USA) was positioned at the same focal distance from the digital camera. No screen was necessary when imaging the CAD/CAM blocks as they acted as the screen. Two blue filters (HOYA UV-VIS bandpass filter; Edmund Optics) and a reflective neutral density filter (Edmund Optics) that was spectrally flat were required to attenuate the light and correct the spectral response of the CCD camera sensor. The camera captured all the images at the same distance, position, and exposure time, thus making the images comparable. The images were collected using the beam analyzer software (BeamGage Professional version 6.14; Ophir-Spiricon, Logan, USA). The control two-dimensional beam profile images used the internal tip diameter (mm) of each LCU, and the "Optical Scaling" tool in the BeamGage Professional

software produced calibrated the beam profile data in millimeters. The mean radiant power values (mW) previously obtained were then entered into the beam analyzer software to create color-coded calibrated tip images of the irradiance in mW/cm<sup>2</sup>. The calibrated data from BeamGage Professional (Ophir-Spiricon) were then exported into OriginPro 2019 version 9.6. (OriginLab; Northampton, USA) where the images were all scaled to the same irradiance levels and x and y dimensions.

#### Light attenuation coefficient

The light attenuation coefficient (AC, mm<sup>-1</sup>) characterizes how quickly incident light is attenuated when passing through a medium.<sup>36,37</sup> The greater the coefficient value, the greater the amount of attenuation, while a small value means that the medium has little effect on light transmission.<sup>36,37</sup> To evaluate the impact of the different specimens on the amount of transmitted light, the attenuation coefficient (AC, mm–1) was based on the Beer-Lambert law:  $I(z) = Io e^{-\alpha z}$ , where IO is the initial light intensity measured in the absence of specimen,  $\alpha$  is the attenuation coefficient, and z is the specimen thickness.

#### Statistical analysis

Radiant power data were analyzed for normal distribution and homoscedasticity using the Shapiro-Wilk and Levene's tests. Three-way ANOVA was used to compare the interactions between study factors: LCUs (3 levels), thicknesses (5 levels), and shades (3 levels) of CAD/CAM material. Multiple comparisons were made using Tukey's post-hoc test. All tests used a significance level of  $\alpha = .05$ , and all analyses were performed using Sigma Plot 13.1 (Systat Software Inc, San Jose, USA). The emission spectra (nm/mW/cm<sup>2</sup>) and beam profiles were analyzed descriptively.

### Results

The mean and standard deviation of radiant power (mW) from the three LCUs and transmitted through the different thicknesses and shades of the slices of CAD-CAM material are reported in Figure 1. The 3-way ANOVA (Table 3) reported that the shade, the thickness of a slice of CAD-CAM material and the LCU had significant effects (p < 0.001). The interaction between the LCU and thickness of the slice of CAD-CAM material, the interaction of LCU and CAD-CAM shade (p < 0.001), the interaction between the thickness and shade of CAD-CAM material (p < 0.001), and also between the LCU, thickness and shade were all significant (p < 0.001). The Tukey test showed that without a slice of the CAD-CAM material, the Valo (VL) LCU transmitted a significantly higher radiant power than EL, and OP delivered a significantly lower radiant power than both EL and OP (p < 0.001). The EL light delivered significantly higher radiant power than VL through the slices of CAD-CAM materials that were 0.5 and 0.75 mm thick, irrespective of the shade (p < 0.001). However, as the thickness increased to 1.0, 1.5 and 2.0 mm, the amount of light transmitted from VL was similar to EL (p = .321). The amount of light transmitted using OP was always significantly lower than from VL and EL, irrespective of the shade (p < 0.001).

The effects of thickness on the radiant power transmitted through the CAD-CAM resin composite for all shades and tested LCUs are shown in Figure 2. The greater the thickness, the lower the radiant power transmitted through the CAD-CAM materials, regardless of the shade and tested LCU (p < 0.001). The bleach shade transmitted the least radiant power through the slices of CAD-CAM material that were 0.5, 0.75 and 1.0 thick (p < 0.001). However, when the slices were 1.5 and 2.0 thick, the Bleach and A2 shades transmitted similar radiant power values (p = .108). The A3.5 shade transmitted the lowest radiant power through the slice of CAD-CAM material, regardless of thickness or tested LCU (p < 0.001).

The spectral radiant power (mW/nm) from the three LCUs without the interposition of a slice of CAD-CAM material (control) is shown in Figure 3. The thickness and shade of the slice of CAD-CAM material significantly affected the light attenuation for all wavelength spectra, irrespective of shade and LCU tested. The slices of CAD-CAM material in the A2 and Bleach shades that were 0.75 mm or greater had a lower attenuation effect on the emission spectrum than A3.5. Figure 3 shows that



\*indicate a significant difference between thickness of the BRAVA CAD-CAM blocks.

**Figure 1.** Means and standard deviations of the radiant power (mW) of each LCU measured using an integrating sphere. Control (without the BRAVA CAD-CAM) and through the three different shades and five different thicknesses of BRAVA CAD-CAM. Different uppercase letters indicate a significant difference between shades. Different lowercase letters indicate significant difference between the LCU used (Tukey test, p < 0.005).

| Table 3. Thee-way ANOVA for the emitted        | radiant power values | (mW) emitted by 3 | LCUs through the | CAD-CAM/RC made in |
|--|----------------------|-------------------|------------------|--------------------|
| three shades and at five different thicknesses | •                    |                   |                  |                    |

| Source of variation     | Sum of squares | DF  | Mean of squares | F         | p-value |
|-------------------------|----------------|-----|-----------------|-----------|---------|
| LCU                     | 1.028.674.158  | 2   | 514.337.079     | 4.996.926 | < 0.001 |
| Thickness               | 560.630.625    | 4   | 140.157.656     | 1.361.670 | < 0.001 |
| Shade                   | 5.076.031.355  | 3   | 16.438.346      | 6.405.920 | < 0.001 |
| LCU x Thickness         | 31.114.954     | 8   | 3.889.369       | 37.786    | < 0.001 |
| LCU x Shade             | 496.749.326    | 6   | 82.791.554      | 804.343   | < 0.001 |
| Thickness x Shade       | 93.334.303     | 12  | 7.777.859       | 75.564    | < 0.001 |
| LCU x Thickness x Shade | 14.603.146     | 24  | 608.464         | 5.911     | < 0.001 |
| Error                   | 12.145.823     | 118 | 102.931         |           |         |

the greater the thickness, the greater the influence on the emission spectrum transmitted through the CAD-CAM material, irrespective of the shade and LCU (p < 0.001). The violet wavelengths from VL were undetectable when the CAD-CAM thickness was 1.0 mm or greater (Figure 3A-C).

The beam profiles for the three LCUs at 0 mm distance are shown in Figure 4. The VL and EL had a more homogeneous beam profile than OM. The light transmission through the slices of the CAD-CAM materials for the three LCUs is shown in Figure 5. The light beam profiles showed that the light transmission was affected by the shade of the CAD-CAM material. The beam profiles show that the light transmission through the A2 shade was greater than Bleach only for 0.5- and 0.75-mm thick slices of CAD-CAM material, irrespective of the LCU tested (Figure 5). The beam profiles of the light transmitted through the shade A3.5 slice of CAD-CAM material was the most negatively affected (Figure 5).



Figure 2. Attenuation (%) of the radiant power from the three LCUs transmitted through five different thicknesses and three shades (Bleach, A2 and A3.5) of BRAVA CAD-CAM.



**Figure 3.** Wavelengths of light (mW/nm) from the LCUs through five different thicknesses of BRAVA CAD-CAM/RC in three shades (Bleach, A2 and A3.5): A-C: VALO Grand; D-F: Elipar DeepCure-S; G-I: Optilight Max.



**Figure 4.** Two- and three-dimensional light beam profiles from the LCUs show the tip diameter and the irradiance (mW/cm<sup>2</sup>) at 0 mm distance without any interposing material. All the images are on the same scale. Note the difference in tip diameters from the 3 LCUs and the 'hot spot' of high irradiance from the Optilight Max and the wider more homogeneous beam profiles for VALO Grand and Elipar DeepCure-S.

The attenuation coefficient of the emitted for the three LCUs with the interposition of a slice of CAD-CAM material for all shades are shown in Figure 6. The attenuation coefficient was higher for lower wavelength (violet light) emitted by VALO Grand and was higher for A3.5 shade than A2 and Bleach shades. As expected, the attenuation is more evident for violet light than for blue light (Figure 6A). As illustrated in Figure 3, the DeepCure-S and the Optilight emitted very little light below 420 nm, and thus the scale for these to LCUs was only extended to 420 nm.

### Discussion

This study evaluated the influence of the thickness and shade of one brand of CAD-CAM material on the light transmission from single-peak and multiple-peak LCUs. The thickness and shade of the low translucency CAD-CAM material significantly influenced the radiant power, attenuation coefficients, and attenuation of the different wavelengths of light. The radiant power, spectral radiant power, attenuation coefficients, and homogeneity of the light emitted from the LCUs were affected differently by the thickness and shade of the Brava Block CAD-CAM material. Thus, the null hypotheses were rejected.

A thickness limit for the restorative material that will allow adequate polymerization of a light-polymerized resin cement should be considered.<sup>12</sup> The amount of light transmitted through the indirect restorative material may need to be increased by increasing the exposure time for the luting cement to be adequately polymerized.<sup>37,11</sup>Otherwise, inadequate polymerization of the luting material can cause postoperative sensitivity, debonding, or staining at the margins, and secondary caries, leading to restoration failure.<sup>15,21</sup>

The greater the thickness of the CAD/CAM material, the lower the transmitted radiant

power (Figure 1). Using a darker shade or a thicker restoration, that is commonly used in endodontically treated or severally structurally

compromised posterior teeth, the greater the amount of light attenuation means that less light will reach the luting resin-based material,<sup>7</sup> and this



**Figure 5.** The two-dimensional representations of the beam profile recorded using the standard light output mode of the LCUs through the five thicknesses and Bleach, A2 and A3.5 shades of the BRAVA CAD-CAM blocks.



**Figure 6.** Light Attenuation Coefficients of the LCUs in relation to the different thicknesses of the different shades of the CAD/ CAM blocks. Note the scale of the Elipar DeepCure-S and the Optilight finish at 420 nm because these lights emit very little light below 420 nm.

can negatively affect the polymerization process. For perpendicularly incident light source and at the closest exposure to the material surface, the amount of light transmitted through a CAD/CAM material decreases exponentially as the specimen thickness increases.7 Consequently, an insufficient amount of light may reach the resin at the bottom of the proximal box in premolars and molars where the light must pass through several mm of CAD/CAM material. This may be the cause of premature failure in these areas that are furthest away from the light source. The conditions evaluated in this study were more challenging because a low translucency CAD-CAM material was used, resulting in more light attenuation than a higher translucency Brava Block, but the LCUs were used under ideal conditions, and the transmission was optimized. This may not always occur in the mouth.

Clinicians should recognize that the shade can significantly affect light transmission through the restorative material. Figure 3 shows that this light attenuation was greater in the Bleach shade, even though it is whiter than A2, and for the darker A3.5 shade. Darker resin composites tend to absorb more light, because the pigments attenuate the light.<sup>30</sup> Thus darker shades require a longer light exposure time, especially as the thickness increases.<sup>14</sup> The bleach shade also had higher light attenuation than the A2 shade. This occurred because the bleach shade has more white pigments and is consequently more opaque. These opaquers probably cause increased light scattering and absorbance compared to more translucent shades, such as A2.<sup>21,29</sup> When the darker and thicker slices of the CAD-CAM material were tested, the attenuation of the light was even more evident (Figures 1, 3 and 6). Therefore, longer exposure times and additional light activation from the buccal and lingual are recommended.

Many variables affect the amount of light energy transmitted through the material, such as the design and tip size of the LCU, spectral irradiance, exposure time, shade, and opacity of the restorative material.<sup>15,16,25</sup> In this study, the emission spectrum was significantly different among the three LCUs tested. With the increasing availability of brands and models of LCUs, the clinician may not know which LCU they should use. They may also base their decision on misleading data such as an averaged irradiance value.<sup>25</sup> In this study, VL delivered the lowest irradiance value because its tip is 12 mm in diameter compared to OP, which has a 7 mm tip (Table 1). Since the radiant exitance is the irradiance (mW/cm<sup>2</sup>) at the light tip is the total radiant power (mW) emitted at the tip divided by the area of the light-emitting tip, this is an averaged radiant exitance (irradiance) value across the entire light tip. Reducing the tip diameter from 10 to 7 mm will halve the tip area and double the irradiance if the same power is delivered. It is not uncommon to

see companies reduce the tip diameter to deliver an irradiance that is equivalent to or even greater than a more powerful higher-cost LCU that has a wider light tip.<sup>25,32</sup> When evaluating the beam profiles, the light from VL and EL sources was more uniform than the light from OP. The radiant exposure values were also higher for VL and EL. In practice, this lack of homogeneity and power can negatively affect the photo-activation of resins, especially at the restoration edges, ultimately leading to failure of the restoration.<sup>9,15,27</sup>

With the tendency to deliver lighter restorations, alternative photoinitiators different from camphorquinone were introduced.<sup>13,19</sup> Most require light in the violet range (below 410 nm) compared to materials that use only CQ, which requires a different wavelength of blue light (around 468-470nm).13 Broad-spectrum multi-peak LCUs have been gaining popularity because they deliver both violet and blue light, and the manufacturers claim they will photoactive all known dental resins.<sup>8,23,20</sup> However, when the wavelengths of light transmitted through the CAD/CAM block were examined, it became evident that the light attenuation increased with increasing resin composite thickness and was much greater for the violet light (Figures 3 and 6). Thus, if the resin cement requires violet light to be optimally cured, this is a problem. It may also be problematic if the clinician chooses to photo-activate a bonding agent that requires violet light through the overlying restorative material. However, some companies have developed resin cements that use Norrish Type I photoinitiators (Ivoclar, Schaan, Liechtenstein) that are more efficient and require fewer photons to produce free radicals than Type II photoinitiators.<sup>38</sup> These Type I photoinitiators do not require co-initiators, they are less yellow in color and have higher absorptivity.

This study shows that the choice of LCU, luting material, shade, thickness of the restoration, and the exposure time all influence the amount of transmitted light. This study has limitations because the light transmission was measured only through flat surfaces of the CAD-CAM material. Another limitation is that only correctly functioning LCUs and one CAD-CAM material were tested in this study. Other products and LCUs may have different outcomes.<sup>7,23,34,35</sup> The operator technique, the light source (LCU), and the direction of light will all affect the amount of light delivered such that the polymerization obtained clinically may sometimes be much less than that achieved under ideal laboratory conditions.<sup>14</sup> Some clinicians use flowable or heated high-viscosity light-activated resin composites to cement their CAD-CAM restoration.<sup>20</sup> This decision should be carefully reconsidered as the thickness of the CAD-CAM material increases. Clinicians should be careful when faced with a clinical situation with greater restoration thickness in hard-to-reach locations, such as second molars, and with dark or white opaque shades.30 A dual-activated resin cement should be used if the restoration is greater than 1 mm thick.11 The clinician should ensure that the light of the LCU has a direct straight-line access to all the surfaces of the restoration, and none of the resin cement should be in shadow.<sup>24</sup>

## Conclusion

Within the limitation of this study, the following conclusions can be drawn:

- a. As the thickness of the tested CAD-CAM material increases, the radiant power and the spectral radiant power of the transmitted light from all tested LCUs decreased exponentially.
- b. The A3.5 shade of the tested CAD-CAM material had higher light attenuation than the Bleach and A2 shades using any of the tested LCUs.
- c. VALO Grand and Elipar DeepCure delivered the most homogenous light and greater radiant power compared to Optilight Max.
- d. The violet light from the VALO Grand multipeak LCU was undetectable when the CAD/ CAM material was 2.0-mm thick.

#### Acknowledgment

This project was funded by grants from CNPq-National Council for Scientific and Technological Development, grants 434598/2018-6 and 406840/2022-9; and FAPEMIG, grants APQ-02105-18. CAPES – grants PrInt-CAPES UFU P4.

### References

- 1. Baba NZ, Goodacre BJ, Goodacre CJ, Müller F, Wagner S. CAD/CAM Complete denture systems and physical properties: a review of the literature. J Prosthodont. 2021 May;30 S2:113-24. https://doi.org/10.1111/jopr.13243
- Wiedenmann F, Klören M, Edelhoff D, Stawarczyk B. Bond strength of CAD-CAM and conventional veneering materials to different frameworks. J Prosthet Dent. 2021 Apr;125(4):664-73. https://doi.org/10.1016/j.prosdent.2020.01.048
- 3. Peumans M, Valjakova EB, De Munck J, Mishevska CB, Van Meerbeek B. Bonding Effectiveness of Luting Composites to Different CAD/CAM Materials. J Adhes Dent. 2016;18(4):289-302. https://doi.org/10.3290/j.jad.a36155
- 4. Ruse ND, Sadoun MJ. Resin-composite blocks for dental CAD/CAM applications. J Dent Res. 2014 Dec;93(12):1232-4. https://doi.org/10.1177/0022034514553976
- Souza J, Fuentes MV, Baena E, Ceballos L. One-year clinical performance of lithium disilicate versus resin composite CAD/CAM onlays. Odontology. 2021 Jan;109(1):259-70. https://doi.org/10.1007/s10266-020-00539-3
- 6. Güth JF, Zuch T, Zwinge S, Engels J, Stimmelmayr M, Edelhoff D. Optical properties of manually and CAD/CAM-fabricated polymers. Dent Mater J. 2013;32(6):865-71. https://doi.org/10.4012/dmj.2013-099
- Butterhof M, Ilie N. Predicting transmitted irradiance through CAD/CAM resin composite crowns in a simulated clinical model. Dent Mater. 2021 Jun;37(6):998-1008. https://doi.org/10.1016/j.dental.2021.03.002
- 8. Price RB, Ferracane JL, Shortall AC. Light-curing units: a review of what we need to know. J Dent Res. 2015 Sep;94(9):1179-86. https://doi.org/10.1177/0022034515594786
- 9. Soto-Montero J, Nima G, Dias CT, Price RB, Giannini M. Influence of beam homogenization on bond strength of adhesives to dentin. Dent Mater. 2021 Feb;37(2):e47-58. https://doi.org/10.1016/j.dental.2020.10.003
- Watts DC, Cash AJ. Analysis of optical transmission by 400-500 nm visible light into aesthetic dental biomaterials. J Dent. 1994 Apr;22(2):112-7. https://doi.org/10.1016/0300-5712(94)90014-0
- 11. Faria-E-Silva AL, Pfeifer CS. Effectiveness of high-power LEDs to polymerize resin cements through ceramics: an in vitro study. J Prosthet Dent. 2017 Nov;118(5):631-6. https://doi.org/10.1016/j.prosdent.2016.12.013
- Pishevar L, Ashtijoo Z, Khavvaji M. The effect of ceramic thickness on the surface microhardness of dual-cured and light-cured resin cements. J Contemp Dent Pract. 2019 Apr;20(4):466-70. https://doi.org/10.5005/jp-journals-10024-2540
- Schneider LF, Ribeiro RB, Liberato WF, Salgado VE, Moraes RR, Cavalcante LM. Curing potential and color stability of different resinbased luting materials. Dent Mater. 2020 Oct;36(10):e309-15. https://doi.org/10.1016/j.dental.2020.07.003
- Leloup G, Holvoet PE, Bebelman S, Devaux J. Raman scattering determination of the depth of cure of light-activated composites: influence of different clinically relevant parameters. J Oral Rehabil. 2002 Jun;29(6):510-5. https://doi.org/10.1046/j.1365-2842.2002.00889.x
- 15. Soares CJ, Faria-E-Silva AL, Rodrigues MP, Vilela AB, Pfeifer CS, Tantbirojn D, et al. Polymerization shrinkage stress of composite resins and resin cements - What do we need to know? Braz Oral Res. 2017 Aug;31 suppl 1:e62. https://doi.org/10.1590/1807-3107bor-2017.vol31.0062
- Rueggeberg FA, Giannini M, Arrais CA, Price RB. Light curing in dentistry and clinical implications: a literature review. Braz Oral Res. 2017 Aug;31 suppl 1:e61. https://doi.org/10.1590/1807-3107bor-2017.vol31.0061
- Araújo Neto VG, Soto-Montero J, Castro EF, Feitosa VP, Rueggeberg FA, Giannini M. Effects of shades of a multilayered zirconia on light transmission, monomer conversion, and bond strength of resin cement. J Esthet Restor Dent. 2022 Mar;34(2):412-22. https://doi.org/10.1111/jerd.12821
- Borges LP, Borges GA, Correr AB, Platt JA, Kina S, Correr-Sobrinho L, et al. Effect of lithium disilicate ceramic thickness, shade and translucency on transmitted irradiance and knoop microhardness of a light cured luting resin cement. J Mater Sci Mater Med. 2021 Jul;32(8):90. https://doi.org/10.1007/s10856-021-06562-2
- Delgado AJ, Castellanos EM, Sinhoreti M, Oliveira DC, Abdulhameed N, Geraldeli S, et al. The Use of Different Photoinitiator Systems in Photopolymerizing Resin Cements Through Ceramic Veneers. Oper Dent. 2019;44(4):396-404. https://doi.org/10.2341/17-263-L
- Bragança GF, Mazão JD, Versluis A, Soares CJ. Effect of luting materials, presence of tooth preparation, and functional loading on stress distribution on ceramic laminate veneers: A finite element analysis. J Prosthet Dent. 2021 May;125(5):778-87. https://doi.org/10.1016/j.prosdent.2020.02.005
- Rodriguez A, Yaman P, Dennison J, Garcia D. Effect of light-curing exposure time, shade, and thickness on the depth of cure of bulk fill composites. Oper Dent. 2017;42(5):505-13. https://doi.org/10.2341/16-057-L
- 22. Schneider LF, Pfeifer CS, Consani S, Prahl SA, Ferracane JL. Influence of photoinitiator type on the rate of polymerization, degree of conversion, hardness and yellowing of dental resin composites. Dent Mater. 2008 Sep;24(9):1169-77. https://doi.org/10.1016/j.dental.2008.01.007

- Effect of thickness and shade of CAD/CAM composite on the light transmission from different light-curing units
- 23. Oliveira DC, Rocha MG, Correa IC, Correr AB, Ferracane JL, Sinhoreti MA. The effect of combining photoinitiator systems on the color and curing profile of resin-based composites. Dent Mater. 2016 Oct;32(10):1209-17. https://doi.org/10.1016/j.dental.2016.06.010
- 24. Soares CJ, Rodrigues MP, Oliveira LR, Braga SS, Barcelos LM, Silva GR, et al. An evaluation of the light output from 22 contemporary light curing units. Braz Dent J. 2017;28(3):362-71. https://doi.org/10.1590/0103-6440201601466
- Price RB, Ferracane JL, Hickel R, Sullivan B. The light-curing unit: an essential piece of dental equipment. Int Dent J. 2020 Dec;70(6):407-17. https://doi.org/10.1111/idj.12582
- 26. Harlow JE, Rueggeberg FA, Labrie D, Sullivan B, Price RB. Transmission of violet and blue light through conventional (layered) and bulk cured resin-based composites. J Dent. 2016 Oct;53:44-50. https://doi.org/10.1016/j.jdent.2016.06.007
- 27. Shimokawa C, Turbino ML, Giannini M, Braga RR, Price RB. Effect of curing light and exposure time on the polymerization of bulk-fill resin-based composites in molar teeth. Oper Dent. 2020;45(3):E141-55. https://doi.org/10.2341/19-126-L
- Mazao JD, Braga SSL, Bragança GF, Zancope K, Price RB, Soares CJ. Effect of the ceramic thickness on the light attenuation, degree of conversion, Knoop hardness, and elastic modulus of four luting resin materials. Oper Dent. 2023 Mar;48(2):226-35. https://doi.org/10.2341/21-195-L
- 29. Paravina RD, Ontiveros JC, Powers JM. Curing-dependent changes in color and translucency parameter of composite bleach shades. J Esthet Restor Dent. 2002;14(3):158-66. https://doi.org/10.1111/j.1708-8240.2002.tb00516.x
- 30. Aguiar FH, Lazzari CR, Lima DA, Ambrosano GM, Lovadino JR. Effect of light curing tip distance and resin shade on microhardness of a hybrid resin composite. Braz Oral Res. 2005;19(4):302-6. https://doi.org/10.1590/S1806-83242005000400012
- Shortall AC, Price RB, MacKenzie L, Burke FJ. Guidelines for the selection, use, and maintenance of LED light-curing units. Part 1. Br Dent J. 2016 Oct;221(8):453-60. https://doi.org/10.1038/sj.bdj.2016.772
- 32. Soares CJ, Braga S, Price RB. Relationship between the cost of 12 light-curing units and their radiant power, emission spectrum, radiant exitance, and beam profile. Oper Dent. 2021 May;46(3):283-92. https://doi.org/10.2341/19-274-L
- 33. Oliveira GU, Mondelli RF, Charantola Rodrigues M, Franco EB, Ishikiriama SK, Wang L. Impact of filler size and distribution on roughness and wear of composite resin after simulated toothbrushing. J Appl Oral Sci. 2012;20(5):510-6. https://doi.org/10.1590/S1678-77572012000500003
- 34. Van der Laan HL, Zajdowicz SL, Kuroda K, Bielajew BJ, Davidson TA, Gardinier J, et al. Biological and mechanical evaluation of novel prototype dental composites. J Dent Res. 2019 Jan;98(1):91-7. https://doi.org/10.1177/0022034518795673
- 35. Masotti AS, Onófrio AB, Conceição EN, Spohr AM. UV-vis spectrophotometric direct transmittance analysis of composite resins. Dent Mater. 2007 Jun;23(6):724-30. https://doi.org/10.1016/j.dental.2006.06.020
- 36. Chang S, Bowden AK. Review of methods and applications of attenuation coefficient measurements with optical coherence tomography. J Biomed Opt. 2019 Sep;24(9):1-17. https://doi.org/10.1117/1.JBO.24.9.090901
- 37. Attenuation coeficiente. In: International Union of Pure and Applied Chemistry. Compendium of chemical terminology, 2nd ed. Oxford: Blackwell; 1997. "
- Kowalska A, Sokolowski J, Bociong K. The photoinitiators used in resin based dental composite-a review and future perspectives. Polymers (Basel). 2021 Feb;13(3):470. https://doi.org/10.3390/polym13030470

ERRATUM

Effect of thickness and shade of CAD/CAM composite on the light transmission from different light-curing unitsBraz Oral Res. 2023;37:e114.

See a correct Figure 6.



https://doi.org/10.1590/1807-3107bor-2023.vol37.0114.erratum

