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# EFFECTS OF SCANDIUM DOPING CONCENTRATION ON THE PROPERTIES OF STRONTIUM COBALT OXIDE MEMBRANES

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**Abstract** - Perovskite-type mixed conducting oxides of  $SrCo_{1-y}Sc_yO_{3-\delta}$  (y=0.02-0.7) were synthesized by a combined EDTA-citrate complexing method. Different scandium doping concentrations in  $SrCo_{1-y}Sc_yO_{3-\delta}$  have significant effects on the phase structure, electrical conductivity, surface properties and oxygen permeation behaviour of the resultant membranes.  $SrCoO_{3-\delta}$  without scandium incorporation displayed a 2H BaNiO<sub>3</sub>-type structure with almost zero oxygen flux at high temperatures. Small amounts of  $Sc_2O_3$  doping (y<0.1) efficiently stabilized the oxide in a cubic perovskite structure, leading to a sharp increase in the permeation flux, with a maximum value of 3.1ml.cm<sup>-2</sup>.min<sup>-1</sup> achieved at  $900^{\circ}$ C for  $SrCo_{0.95}Sc_{0.05}O_{3-\delta}$  and  $SrCo_{0.9}Sc_{0.1}O_{3-\delta}$  membranes. The permeation process could be rate-limited by either the oxygen bulk diffusion, oxygen surface exchange, or a combination of both depending on the scandium doping level. Further increases of the  $Sc^{3+}$  doping concentration (y>0.1) were found to lower the membrane oxygen fluxes, with  $y\ge0.4$  doped  $SrCo_{1-y}Sc_yO_{3-\delta}$  ceramics no longer showing any oxygen permeation. *Keywords*: Perovskite; Mixed conduction; Oxygen separation membrane; Rate limiting.

#### INTRODUCTION

Oxygen is one of the most important chemicals used in industry today. Up to now, it is mainly produced from the cryogenic distillation of air, which is only economically attractive for large-scale applications. A potential alternative technique is through the use of ceramic oxygen permeating membranes (Kovalevsky et al., 1998; Tong et al., Ishihara et al., 2002), which are composed of mixed ionic and electronic conducting (MIEC) oxides. Such membranes have 100% oxygen permeating selectivity (Tsai et al., 1997; Shao et al., 2001; Shaula et al., 2003; Lu et al., 2006; Fagg et al., 2007). The

envisaged advantages of oxygen production via ceramic membrane technology include high size-flexibility, and capability for continuous production of oxygen with substantial reductions in energy consumption (Hendriksen et al., 2000; Bouwmeester, 2003). However, the successful application of the MIEC membrane technology in the oxygen industry strongly depends on the development of high-performance membranes.

Oxygen permeation flux is one of the most important parameters of this technology and is usually considered first in the development of MIEC membranes for commercial application purposes (Tsiakaras et al., 1998; Yaremchenko et al., 1999).

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Different from porous ceramic membranes, for which the gas permeability is very structurally dependent (such as pore size and pore size distribution); the oxygen permeability of MIEC membranes is more material-related. Therefore, the development of new materials with high oxygen permeability and phase stability has been the major effort of most researchers in the related field (Bouwmeester, et al., 1992; Shao et al., 2001; Diethelm et al., 2003; Qi and Lin, 2003; Diethelm and Van Herle, 2004; Deng et al., 2004; Kim et al., 2005; Schiestel et al., 2005).

MIEC ceramic materials usually have defined phase structures, which can be derived from perovskite, brownmillerite, fluorite, and others (Kruidhof et al., 1993; Shao et al., 2000; Kharton et al., 2001, 2002; Wiik et al., 2002; Fan et al., 2007). Among them, the perovskite membranes exhibit the highest permeability and greatest potential for improvement [Boginsky, 1998; Ishihara et al., 2000; James et al., 2004]. The doping strategy has been widely applied to improve the permeation properties of the perovskite membranes with dopant choice and dopant level having a significant effect on the lattice structure, electrical conductivity, sintering behaviour, oxygen permeation flux, and even the rate-determining step of the membranes (Zhu et al., 2004; Tong et al., 2003; Trofimenko et al., 1997; Zeng et al., 2007, 2008).

Recently we have demonstrated SrSc<sub>0.05</sub>Co<sub>0.95</sub>O<sub>3-δ</sub> is a promising material for oxygen permeating membranes, showing high oxygen permeability at high temperatures (Zeng et al., 2007). Inspired by this finding, our research work in this study is on further developing scandium doped SrCoO<sub>3-8</sub> for ceramic membrane applications, investigating a series of composite oxides with the nominal composition of  $SrCo_{1-v}Sc_vO_{3-\delta}$  (y=0~0.7), achieved by varying the scandium doping level on the B-site. The impact of Sc<sup>3+</sup> doping level on the oxygen permeability and the rate-determining step(s) of the membranes is emphasized in this study.

# **EXPERIMENTAL**

# SrCo<sub>1-v</sub>Sc<sub>v</sub>O<sub>3-δ</sub> Powder and Membrane Synthesis

 $SrCo_{1-y}Sc_yO_{3-\delta}$  (y=0~0.7) (SCSy) composite oxides were synthesized by a combined EDTA-citrate complexing sol-gel process with  $Sr(NO_3)_2$ ,  $Co(NO_3)_2$ , and  $Sc(NO_3)_3$  as the raw materials for the metal-ion sources. The detailed information about this wet-chemical process can be found elsewhere

(Shao et al., 2000). Stoichiometric amounts of the metal nitrates were added to an EDTA-NH<sub>3</sub>.H<sub>2</sub>O aqueous solution under heating and stirring, followed by the addition of citric acid as the second chelant. The pH value of the system was controlled at 6 by the addition of NH<sub>4</sub>OH during the whole gel formation process to avoid the deposition of individual metal ions. With the evaporation of water, dark purple gels were obtained, which were preheated at 250°C for several hours to form solid precursors and then calcined at 900°C in air for 5 h to obtain the oxides with the aimed composition and lattice structure.

The prepared powders were grounded in a high-energy ball mill (Fritsch, Pulverisette 6), and subsequently pressed into disks or bars by stainless steel dies with a diameter of 15mm or dimensions of 5mm×8mm×25mm under a hydraulic force of 30ton. These green disks or bars were sintered to dense bodies at  $1100^{\circ}$ C for 5h, respectively. The sintered membranes have a diameter of 12-13mm and thickness of 0.7-1.0mm, while the sintered bars have a dimension of 3mm×5mm×20mm. The densities of these membranes were measured by the Archimedes liquid displacement technique. The gas tightness of the membranes was examined by the detection of  $N_2$  leakage analysed by gas chromatography.

# Characterization

The phase structure of the samples was investigated using an X-ray Diffractometer (Bruker D8 Advance) with Cu K $\alpha$  radiation. The experimental diffraction patterns were collected at room temperature by step scanning in the range of  $10^{\circ} \le 20 \le 90^{\circ}$ . The morphological features of the prepared membranes were examined using an Environmental Scanning Microscope (ESEM, QUANTA-2000). The room temperature oxygen non-stoichiometry was measured by the iodometric titration technique.

The electrical conductivity was measured by the four-probe D. C. method on sintered bars in air upon cooling from 900°C to 300°C at 5°C per step. Silver paste was painted on the square cross sectional edges of the sample or along the rectangular edges (separated by a distance L) to form current and voltage electrodes. Two silver wires acted as current contacts and another two sliver wires acted as the voltage contacts, which were attached to the electrodes using silver paste. The sample was placed in a vertical split tube furnace. A constant current was applied to the two current wires and the voltage response on the two voltage wires was recorded using a Keithley 2420 sourcemeter. The current was

increased from 1uA to a maximum value of 2A.

Dense Sm<sub>0.15</sub>Ce<sub>0.85</sub>O<sub>1.925</sub> pellets with diameter of 12.9mm and thickness of 1.0mm, produced by dry pressing followed by sintering at 1350°C for 5h, were applied as the electrolyte substrates for the impedance test of the membrane materials. Two nominally identical electrodes (1.21cm<sup>2</sup>) made from the membrane materials, with a thickness of  $\sim 10 \mu m$ and porosity of  $\sim 35\%$ , were deposited on each side of the electrolyte pellet by painting method and calcined at 1000°C for 5h in air. Impedance measurements performed were using electrochemical workstation based on a Solartron 1260A frequency response analyser in combination with a Solartron 1287 Potentiostat/Galvanostat. The two-electrode cells were tested at open circuit voltage. In general, the electrochemical tests were performed from 850°C to 500°C in 25°C intervals in air, in the frequency range of 0.01- 105Hz and applied AC voltage amplitude of 10mV.

# **Oxygen Permeation Study**

Oxygen permeation properties of the membranes were investigated using a high-temperature oxygenpermeation apparatus as shown in Figure 1. Both surfaces of the membranes were carefully polished using a 1000 mesh SiC sand paper to a thickness of 0.91 mm and sealed to quartz tubes with silver paste. The effective membrane area for permeation study is 0.45cm<sup>2</sup>. The oxygen permeation properties were investigated using the gas chromatographic method by applying ambient air as the feed side atmosphere and helium as the sweep gas to carry the permeated oxygen to a Varian 3800 gas chromatograph equipped with a 5Å molecular sieve capillary column for in-situ gas composition analysis. All values of oxygen permeation fluxes or other gas flowrates mentioned in this paper were calculated at the conditions of standard temperature and pressure (STP).

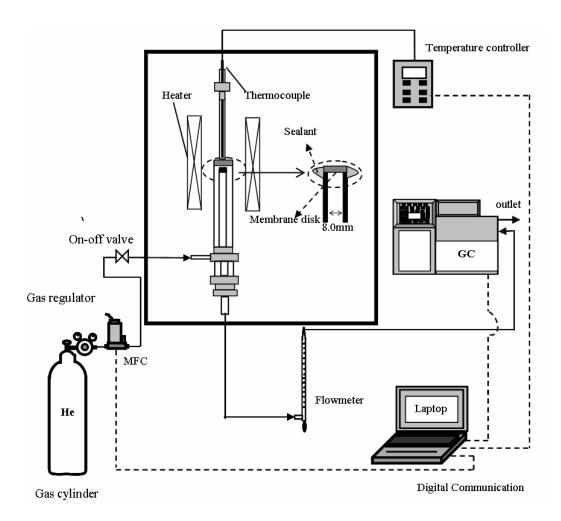


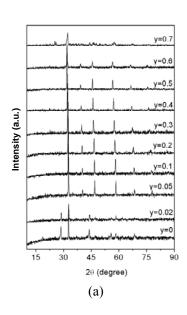
Figure 1: The set-up for the oxygen permeation measurement

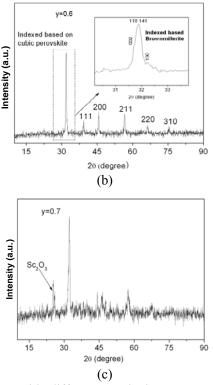
#### RESULTS AND DISCUSSION

# **Basic Characterization of the Oxide Powders**

Figure 2 shows the XRD patterns of the SCSy oxides  $(0 \le y \le 0.7)$ , prepared by calcinations of their solid precursors at 850°C in air for 5h. The parent oxide of  $SrCoO_{3-\delta}$  (SC) and the oxides with very low scandium doping concentration, for example SCS0.02 (y=0.02), demonstrated a typical 2H BaNiO<sub>3</sub>-type structure. Oxide SCS0.02 changed to a brownmillerite structure when the firing temperature was elevated to 1100°C. However, at higher doping concentrations in the range of 5 to 50mol.% (y=0.05-0.5), the oxides changed to a cubic perovskite lattice structure. A co-existence of perovskite and brownmillerite phases was observed when the doping amount rose to 60mol.% (Figure 2b), while un-reacted Sc<sub>2</sub>O<sub>3</sub> oxide was detected for an apparent composition of SrCo<sub>0.3</sub>Sc<sub>0.7</sub>O<sub>3-δ</sub> (Figure 2c). Since the brownmillerite structure is an oxygen vacancyordered structure of the cubic perovskite, together with the fact that no Sc<sub>2</sub>O<sub>3</sub> impurity phase was detected at y=0.6, the solubility limit of  $Sc^{3+}$  in SrCoO<sub>3-δ</sub> parent oxide is believed to be around

60mol.%, which is higher than that reported by Maignan et al. (~ 40mol.%) in 2004. This discrepancy may result from the different synthetic methods used. The cubic perovskite structure of SCSy (y=0.05-0.5) was found to be stable from room temperature to high temperature under oxygen, air and argon atmosphere, indicating their potential application as oxygen separation membrane. The lattice parameters of all the samples are shown in Table 1. It clearly shows a cell expansion with the increase of Sc<sup>3+</sup> doping concentration, which is well understood since Sc<sup>3+</sup> (+0.745Å) is larger in ionic radius size than the cobalt ions (Co<sup>3+</sup>, 0.545Å (LS), 0.61Å (HS), and  $\text{Co}^{4+}$ , 0.53Å) at the B-site of perovskite. As shown in Table 1, the oxygen nonstoichiometry increases gradually with the scandium doping level. The average valence state of cobalt ions was then calculated based on the obtained corresponding oxygen non-stoichiometry, which decreases gradually with the scandium doping concentration, which is opposite to the case of SrCo<sub>1</sub>.  $_{v}$  Nb $_{v}$ O $_{3-\delta}$  (Zhang et al., 2008). In the table above, the results suggest that the physical properties of cobalt ions in perovskite are highly sensitive to the type of dopant used.





**Figure 2:** X-ray diffraction patterns of  $SrCo_{1-y}Sc_yO_{3-\delta}$  oxides with different Sc doping concentration (y=0~0.7) calcined at 850°C (a); Magnified x-ray diffraction patterns of  $SrCo_{0.4}Sc_{0.6}O_{3-\delta}$  oxide (b) and  $SrCo_{0.3}Sc_{0.7}O_{3-\delta}$  oxide (c) with more details

 $V^* (A^3)$ d(Å) Symmetry δ 0.05 3.8704(2) 57.977(0) 3.074(3) 0.465(4)Pm3m 58.515(2) 3.8823(4) 3.056(2)0.1 Pm3m 0.475(2)0.2 Pm3m 3.9008(5) 59.357(6) 2.882(5) 0.547(5)0.3 Pm3m 3.9213(0) 60.296(2) 2.688(6)0.609(1)0.4 3.9401(3) Pm3m 2.620(0)0.614(3)61.167(6) 0.5 Pm3m 3.9697(2) 62.556(7) 2.528(0)0.618(0)

Table 1: Lattice constants (d), oxygen nonstoichiometry ( $\delta$ ) and the average oxidation state of cobalt (x) of the SCSy samples (y=0.05-0.5)

\*Unit cell volume

The electrical conductivity of the oxides in air at various Sc3+ doping concentrations, as measured by the 4-probe DC conductivity method, is shown in Figure 3. SrCoO<sub>3-8</sub> shows a medium level of electrical conductivity between 300 and 900°C. It increased monotonically from about 3S.cm<sup>-1</sup> at 300°C to 30S.cm<sup>-1</sup> at 900°C. A minor amount of Sc<sup>3+</sup> doping into SrCoO<sub>3-8</sub> resulted in a substantial increase of the electrical conductivity. The maximum values were reached at a  $Sc^{3+}$  doping concentration of 5mol.% (y=0.05), with higher levels of Sc<sup>3+</sup> causing a sharp decrease in the electrical conductivity measured. For example, at 850°C, the electrical conductivity is 23.6, 72, 60.2, 21.6, 5.7 and 0.85S.cm<sup>-1</sup> in air, respectively, for SCSy with y=0, 0.05, 0.1, 0.2, 0.3 and 0.4. The electrical conductivity is almost zero at  $y \ge 0.5$ . When the Sc<sup>3+</sup> doping concentration is in the range of 0.02 to 0.1. the electrical conductivity first increased with temperature then decreased, while a monotonic increase of electrical conductivity with temperature was observed for the others.

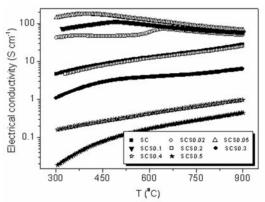


Figure 3: Electrical conductivities of SCSy  $(y=0\sim0.5)$  under air atmosphere

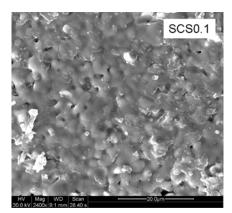
It is well known that, in the perovskite oxide, the electron conduction is created by B-site lattice cations through strongly overlapping B-O-B bonds with a mechanism like the Zerner double exchange

process (Zerner, 1951). The electrical conductivity is closely related with the phase structure and the redox capability of the B-site cations. Since the SrCoO<sub>3-δ</sub> parent oxide showed a distorted 2H BaNiO<sub>3</sub>-type phase structure, the Zerner double exchange of an electron between B-site lattice cations was significantly inhibited due to the inefficient overlap. The minor amount of Sc<sup>3+</sup> doping resulted in the transition of the phase to a cubic perovskite structure. The 180° overlap between the outer electron orbital of the B-site metal ions and oxygen ion in the cubic perovskite then greatly facilitates the electron conduction. On the other hand, Sc<sup>3+</sup> has a fixed valence state, which acts as a block for the Zerner double exchange of electrons between cobalt ions and oxygen. Therefore, a decrease of electrical conductivity was observed with the increase of Sc<sup>3+</sup> doping amount at y≥0.1. The decreased concentration of the charge carrier also contributed to the reduced electrical conductivity with  $Sc^{3+}$  at y $\geq$ 0.05. Near zero electrical conductivity at y≥0.4 suggests that the Zerner double exchange between cobalt ions and oxygen was totally blocked by the dilution effect of  $Sc^{3+}$ .

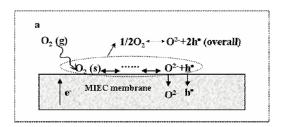
#### **Membrane Performances**

To be applied as mixed conducting oxide membranes, the ceramics must be densified to be gastight and display high oxygen permeation fluxes. SCSy pellets with different Sc concentrations (y=0.0-0.6) were sintered at 1100°C for 5hr. Except for SCS0.02 which shows serious crack formation, all the other samples can be sintered well with complete gastightness and relative density higher than 90% as measured by the Archimedes method. Figure 4 shows a typical SEM picture of the sintered SCSy membrane with y=0.1. The membrane has grain size of about 4 microns. The crack formation in SCS0.02 disks might be related with the phase transition as indicated in its XRD pattern of Figure 2(a). The phase transition may introduce large internal stress during the heating and cooling process.

The oxygen permeation fluxes of SCSy membranes with varying Sc<sup>3+</sup> doping concentration (y=0.0-0.7) between 700 and 900°C are shown in Figure 5. All the membranes were controlled at the same thickness of 0.91mm and their surfaces were polished by 1000mesh SiC sand papers to ensure similar surface morphology. SC membranes show very low permeability between 700 and 900°C, with a measured permeation flux of only 0.004mL. cm<sup>-2</sup>. min<sup>-1</sup> at 900°C, which is at the lower detection limit by the GC method. A minor amount of Sc<sup>3+</sup> doping into the structure of SC, however, resulted in a significant increase in the oxygen permeation flux of the membrane. For example, it reached as high as 3.1mL.cm<sup>-2</sup>.min<sup>-1</sup> at 900°C for SCS0.05 membrane. However, the permeation flux of SCS0.02 failed due to the serious crack formation of the membrane. The SCS0.1 membrane shows comparable permeation flux to that of the SCS0.05 membrane, though the permeation flux deteriorated seriously with any further increase of Sc<sup>3+</sup> doping concentration. For example, a permeation flux of 1.7, 0.7, 0.07mL.cm<sup>-</sup> <sup>2</sup>.min<sup>-1</sup> was observed at 900°C for SCS0.2, SCS0.3 and SCS0.4 membranes, respectively. In contrast, no permeation flux was detected for the membranes with Sc<sup>3+</sup> doping concentration of 0.5 or higher, over the whole range of 700-900°C. The oxygen

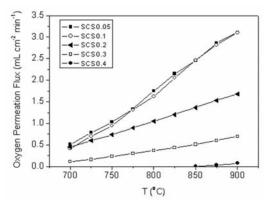


**Figure 4:** SEM image of SCSy (y=0.1) membrane sintered at 1150°C

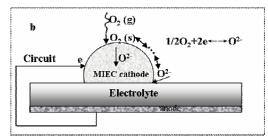


separation through a mixed conducting membrane involves the oxygen exchange over the membrane surfaces (both the feed side and the helium sweep side), and oxygen diffusion and electron transfer through the membrane bulk. Either or both of them could be the rate-determination step.

Electrochemical impedance spectroscopy (EIS) was introduced for assisting the determination of the rate-limiting step(s) of oxygen permeation through SCSy membranes. Figure 6 schematically compares the oxygen reduction over the SCSy electrode based on a symmetric cell configuration and over the MIEC membrane surface. For both cases, they involve the gas phase diffusion, the oxygen surface adsorption, and the dissociation of the oxygen into an oxygen ion and an electron hole over the surface. The dissociated oxygen ions and electron holes migrate through the membrane bulk to the other side of membrane surface of the ceramic membranes, while they incorporate into the electrolyte layer for the symmetric cells. The EIS technique can separate the resistance to oxygen activation over the electrode surface and the resistance to oxygen diffusion through the electrolyte layer. Therefore, the information about the oxygen activation over the electrode can be applied to simulate that on the oxygen permeation membrane surface.



**Figure 5:** Temperature dependence of oxygen permeation fluxes through SCSy membranes with different Sc doing concentration (y=0.05~0.4) membranes under an air/helium gradient



**Figure 6:** A schematic comparison of oxygen reduction (a) over the surface of MIEC membrane, and (b) over the electrode based on symmetric cell

It should be mentioned that, in addition to the oxygen reduction over the electrode surface, sometimes the resistance to oxygen diffusion inside the electrode bulk may also be embodied in the ASRs obtained by EIS. The linear relationship of ASRs with 1000/T strongly suggests that the mechanism for oxygen reduction over SCSv electrodes did not change with temperature or scandium doping concentration. The activation energy for oxygen reduction then calculated based on the temperature dependence of ASRs is 156, 126, 106, 108, 118, 114, 111, and 109kJ.mol<sup>-1</sup> respectively, for SCSy with y=0.0, 0.05, 0.1, 0.2, 0.3, 0.4, 0.5 and 0.6. The activation energy for oxygen bulk diffusion through SCS0.05 is lower than 62.1kJ. mol<sup>-1</sup> (Zeng et al., 2007), while a similar activation energy of 106~120kJ.mol<sup>-1</sup> was observed for SCSy with y varied from 0.05 to 0.6, based on the symmetrical cell test. It suggests that the oxygen surface exchange is the rate-limiting step for oxygen reduction over the SCSy electrodes. Therefore, the obtained ASRs can be reasonably applied to the surface exchange process of ceramic oxygenpermeating membranes.

# a) SrCoO<sub>3-δ</sub> Membrane

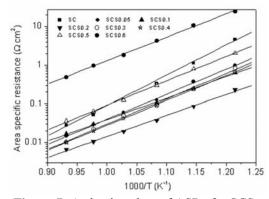
As demonstrated in Figure 7,  $SrCoO_{3-\delta}$  shows good activity for oxygen reduction. Since zero oxygen permeation flux was actually detected, the rate of the permeation process through the SC membrane is likely determined by the slow bulk diffusion processes (oxygen or electron). Under the bulk diffusion process, the permeation flux can be expressed by:

$$J_{O_{2}} = -\frac{RT}{4^{2}F^{2}L} \int_{\ln P_{O_{2}}^{'}}^{\ln P_{O_{2}}^{'}} t_{ion} t_{el} \sigma_{total} d[\ln P_{O_{2}}]$$
 (1)

where  $P_{O_2}$ ,  $P_{O_2}$  are the oxygen partial pressures at the oxygen feed side atmosphere and sweep side atmosphere,  $t_{ion}$  is the oxygen ion transference number,  $t_{el}$  is the electron transference number, and  $\sigma_{total}$  is the sum of electronic conductivity and oxygen ionic conductivity.

The measured electronic conductivity of SrCoO<sub>3-δ</sub> reached 16-30 S.cm<sup>-1</sup> between 700-900°C. Since the oxygen ionic conductivity is typically less than 1S.cm<sup>-1</sup>, the electronic conductivity is then overwhelming. It suggests that the oxygen bulk diffusion is the main rate-limiting step in oxygen

permeation through SC membrane. It is well known that the 2H BaNiO<sub>3</sub>-type structure is a distorted and oxygen vacancy-ordered structure. This structural distortion and vacancy ordering immobilizes the oxygen ion, resulting in negligible oxygen permeation flux for the membrane.



**Figure 7:** Arrhenius plots of ASRs for SCSy (y=0.0-0.6) in air between 550 and 800°C

# b) SCS0.05 and SCS0.1 Membranes

As shown in Figures 4 and 5, both membranes possess considerable high electrical conductivities and oxygen permeation fluxes at high temperatures. In previous works, we have demonstrated that the rate of oxygen permeation through the SCS0.05 membrane was determined mainly by the slow oxygen surface exchange kinetics at the conditions of reduced temperature and low oxygen partial pressure of the sweep side atmosphere (Zeng et al., 2007). The transition of the rate-limiting step from bulk oxygen diffusion of the SC membrane to surface exchange of the SCS0.05 membrane is closely related to the sharp increase of the oxygen mobility inside the lattice due to the formation of cubic perovskite structure upon the Sc<sup>3+</sup> doping.

The rate-limiting step information can be obtained based on the activation energies (Ea) for oxygen permeation. The activation energy for surface exchange is typically higher than that for oxygen bulk diffusion since the dissociation of oxygen to oxygen ion is much more difficult than the diffusion of oxygen. Table 2 shows the Ea for oxygen permeation through SCSy membranes at different temperatures at fixed  $P_{O_2}^{'}$  of 0.21atm and  $P_{O_2}^{''}$  of 0.0148, 0.0078 and 0.00276atm, respectively, for y=0.1, 0.2 and 0.3. For all of them, Ea increased with the decrease of the investigated operational

temperature range. When the temperature zone is

750-800°C, the Ea for oxygen permeation through SCS0.1 membrane is around 110kJ.mol<sup>-1</sup>, which is similar to the activation energy for the oxygen surface exchange process (106kJ.mol<sup>-1</sup>), derived based on the temperature dependence of ASRs. It suggests that the rate of the oxygen permeation process for SCS0.1 membrane at 750-800°C is mainly determined by the surface oxygen exchange. The decrease of Ea with the increase of operating temperatures suggests that the role of bulk diffusion in the rate-determinating step of the oxygen permeation process is strengthened. It is due to the large improvement of surface exchange kinetics compared to the respective improvement in oxygen bulk diffusion rate with temperature. The above results suggest that the oxygen permeation process for SCS0.1 was rate-limited by the relatively slow oxygen surface exchange kinetics at low operation temperatures (<800°C), while it is a combination of oxygen surface exchange and oxygen bulk diffusion at higher temperatures (>800°C).

# c) SCS0.2 and SCS0.3 Membranes

Both of these materials show a medium level of electrical conductivity and oxygen permeability as shown in Figures 4 and 5. Based on the EIS results, however, they possess an improved surface activity for oxygen reduction relative to SCS0.05 and SCS0.1. The obvious deterioration of oxygen permeation fluxes for both SCS0.2 and SCS0.3 membranes, as compared with SCS0.05 and SCS0.1 membranes, suggests that the role of oxygen bulk diffusion in the rate-determinating step is strengthened for SCS0.2 and SCS0.3 membranes.

The Ea for oxygen permeation through SCS0.2 membrane at different temperatures is also shown in Table 2. The apparent Ea was found to increase with the decrease of the temperature. However, the maximum Ea at 750-800°C was only 75.81kJ.mol<sup>-1</sup>, which is much lower than the activation energy for the oxygen surface exchange process (108kJ.mol<sup>-1</sup>), as derived based on the temperature dependence of area specific resistance. It suggests that the oxygen permeation rate through SCS0.2 membrane between 750 and 800°C is determined by the combination of oxygen bulk diffusion and the oxygen surface exchange. The decrease of Ea with temperature implies the enhanced importance of the role of bulk oxygen diffusion in the rate-determinating step. The rate-determination information can also be obtained

from the  $\ln \frac{P_{o_2}^{'}}{P_{o_2}^{"}}$  dependence of permeation flux. As

shown in Figure 8, the permeation flux at  $800^{\circ}$ C gradually increased with the increase of  $\ln \frac{P_{o_2}^{'}}{P_{o_2}^{"}}$ ,

suggesting that the oxygen bulk diffusion has an important role in the rate determination of the oxygen permeation process at 800°C (Zeng et al., 2007). However, at 750°C, the permeation flux

initially increases with the increase of  $ln\frac{P_{o\,2}^{'}}{P_{o_2}^{''}}$  , and

then decreases with the further increase of  $\, ln \frac{P_{o_2}^{'}}{P_{o_2}^{''}} \, .$ 

This suggests that the oxygen surface exchange starts to play an important role in the rate determination of oxygen permeation through SCS0.2 membrane at 750°C.

The higher surface activities, but poorer oxygen permeability, strongly suggests a lower oxygen bulk diffusion rate in SCS0.2 than in SCS0.1. Since SCS0.2 has higher oxygen vacancy concentration than SCS0.05, the defect-association is more likely to occur in SCS0.2. The increased surface activity and reduced bulk diffusion rate then account for the enhanced role of oxygen bulk diffusion in the rate-determination of the oxygen permeation through SCS0.2 membrane.

The electrical conductivity of SCS0.3 was only 1.1~6.3S.cm<sup>-1</sup> between 300~900°C, which is even lower than that of SC due to the blocking effect of Sc<sup>3+</sup> on Zerner double exchange between cobalt ions and oxygen. As shown in Figures 4 and 5, both the surface activities for oxygen reduction and the permeation fluxes of the membranes decreased, as compared to the SCS0.2 membrane. As shown in Table 2, the activation energy for oxygen permeation through SCS0.3 membrane is about 90kJ.mol<sup>-1</sup>, which is lower than that for oxygen surface exchange of 114kJ.mol<sup>-1</sup>. It suggests that the rate of the oxygen permeation process through SSC0.3 membrane is also likely to be determined by a combination of surface exchange and bulk diffusion with an increasing importance of bulk diffusion with temperature.

Under bulk diffusion control of the permeation process, the permeation flux through mixed conducting membranes can be simplified to:

$$J_{O_2} = -\frac{RT}{4^2 F^2 L} \int_{\ln P_{O_2}}^{\ln P_{O_2}} \sigma_{ion} d[\ln P_{O_2}]$$
 (2)

The relationship of  $\sigma_{ion}$  and oxygen partial pressure can be followed by the empirical equation:

$$\sigma_{\text{ion}} = \sigma_{\text{ion}}^{0} P_{\text{O2}}^{n} \tag{3}$$

Combining equations (2) and (3) gives:

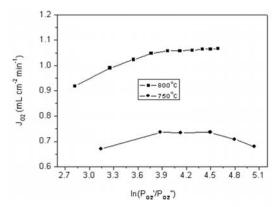
$$J_{O2} = \frac{\beta}{d} [P_{O2}^{"n} - P_{O2}^{'n}] = a[P_{O2}^{"n} - P_{O2}^{'n}]$$
 (4)

where 
$$\beta = -\frac{\sigma_{ion}^{o} RT}{4^{2} F^{2} n}$$
,  $P'_{O2} = 0.21$ atm

Figure 9 shows the PO2" dependence of oxygen permeation fluxes through SCS0.3 membrane at 900oC. A positive value (0.167) of n was observed at PO2"=0.002-0.005atm, while a negative value of n (-0.428) was found at PO2"=0.005-0.017atm. Since both the rate of diffusion through oxygen vacancy sites and the concentration of oxygen vacancies increase with the decrease of oxygen partial pressure, a negative value of n would be predicted if oxygen bulk diffusion is the rate-limiting step based on Eqs.4. The positive value of n at lower PO2" (i.e., 0.002-0.005atm) indirectly suggests that oxygen permeation was mainly determined by oxygen surface exchange, or a combined oxygen surface exchange and oxygen bulk diffusion at large oxygen partial pressure gradient across the 0.91mm thick SCS0.3 membrane.

# d) SCS0.4, SCS0.5, and SCS0.6 Membranes

For SCS0.4, the measured electrical conductivity is less than 1.0S.cm<sup>-1</sup> in air and less than 0.02 S cm<sup>-1</sup> in nitrogen between 500 and 900°C. The oxygen permeation flux of the SSC0.4 membrane is only 0.073, 0.03 and 0.0092mL.cm<sup>2</sup>.min<sup>-1</sup> at 900, 875 and 850°C, respectively. As compared to the SCS0.3 membrane, the oxygen permeation flux of the SCS0.4 membrane decreased sharply. Since the ASRs of SCS0.4 are comparable to that of SCS0.3, the oxygen bulk diffusion becomes the main ratelimiting step for the SCS0.4 membrane. It implies that the increase of scandium doping level from y=0.3 to y=0.4 sharply reduces the oxygen bulk diffusion rate. It is well known that the dopingrelated disorder induces fluctuations of the elastic as well as the coulomb potential in the crystal lattice and thus creates trapping centres for the anion vacancies, which deteriorate the oxygen mobility in the oxide. The increase of  $Sc^{3+}$  doping level to y=0.4 thus seriously deteriorated the oxygen mobility. With the further increase of Sc<sup>3+</sup> doping concentration, zero oxygen permeation flux was obtained. This suggests that the oxygen ion was wholly immobilized, similar to the case of undoped SrCoO<sub>3</sub>. δ. The near zero electrical conductivity implies that, besides oxygen bulk diffusion, electronic conduction may also play a role in the oxygen permeation process, which is different from the case of a  $SrCoO_{3-\delta}$  membrane.

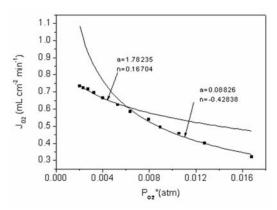


**Figure 8:**  $\ln \frac{P_{o_2}^{'}}{P_{o_2}^{"}}$  dependence on the oxygen permeation fluxes though SCS0.2

membrane at 800 and 750°C with ambient air as the feed side atmosphere

Table 2: Activation Energies for oxygen permeation through SCS0.1, SCS0.2 and SCS0.3 membranes with d=0.91mm,  $P_{O2}'$ =0.21atm,  $P_{O2}''$ =0.0148atm, 0.0078atm and 0.00276atm, respectively.

Temperature range (°C)		750-800	800-850	850-900
Ea	y=0.1	110.0±3.0	96.6±2.3	80.5±1.9
(kJ.mol <sup>-1</sup> )	y=0.2	75.8±1.0	68.3±0.7	60.1±0.5
	y=0.3	92.6±0.7	89.9±1.3	89.6±2.4



**Figure 9:** The P<sub>O2</sub>" dependence of oxygen permeation fluxes through SCS0.3 membrane at 900°C with ambient air as the feed side atmosphere

# **CONCLUSIONS**

A series of SrCo<sub>1-v</sub>Sc<sub>v</sub>O<sub>3-δ</sub> (y=0~0.7) oxides was prepared by a combined EDTA-citrate complexing sol-gel process. A single phase perovskite with a cubic lattice structure was obtained at v≤0.6. The membrane made from undoped parent SC oxide shows near zero permeation flux. Small amounts of Sc<sup>3+</sup> efficiently stabilized the cubic perovskite structure and resulted in a sharp increase of the permeation flux. SCS0.05 and SCS0.1 membranes showed the highest oxygen permeation flux among the doped membranes with a maximum flux of  $\sim 3.1 \text{ mL.cm}^{-2}.\text{min}^{-1}$  at  $900^{\circ}\text{C}$ . At  $y \ge 0.1$ , the permeation flux started to decrease sharply with the increase of Sc<sup>3+</sup> doping amount. The oxygen bulk diffusion was the rate-determining step for the SC membrane, while the SCS0.05 and SCS0.1 membranes were actually rate-limited by the relatively slow oxygen surface exchange kinetics at low operation temperatures (<800°C). further increase of Sc<sup>3+</sup> doping concentration, the importance of bulk diffusion in the rate-determining step is enhanced, with a combination of rate limiting oxygen surface exchange and bulk diffusion for the case of both SCS0.2 and SCS0.3 membranes. At y≥0.4, the permeation process was again mainly ratelimited by the slow oxygen bulk diffusion.

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